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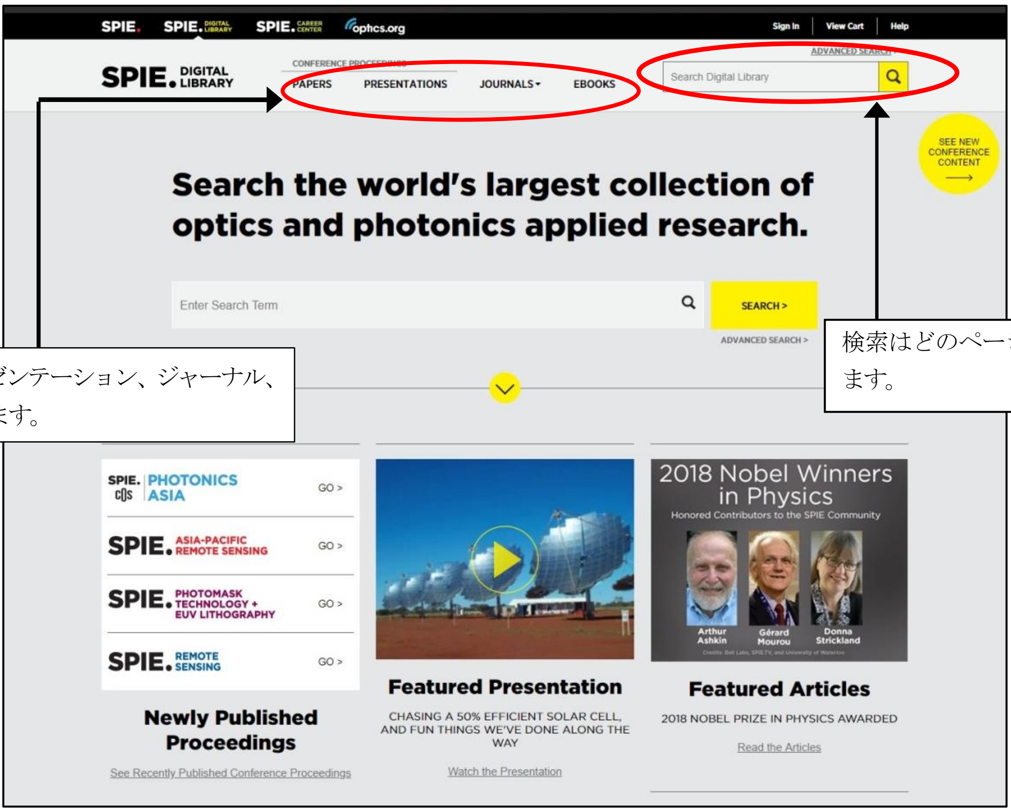

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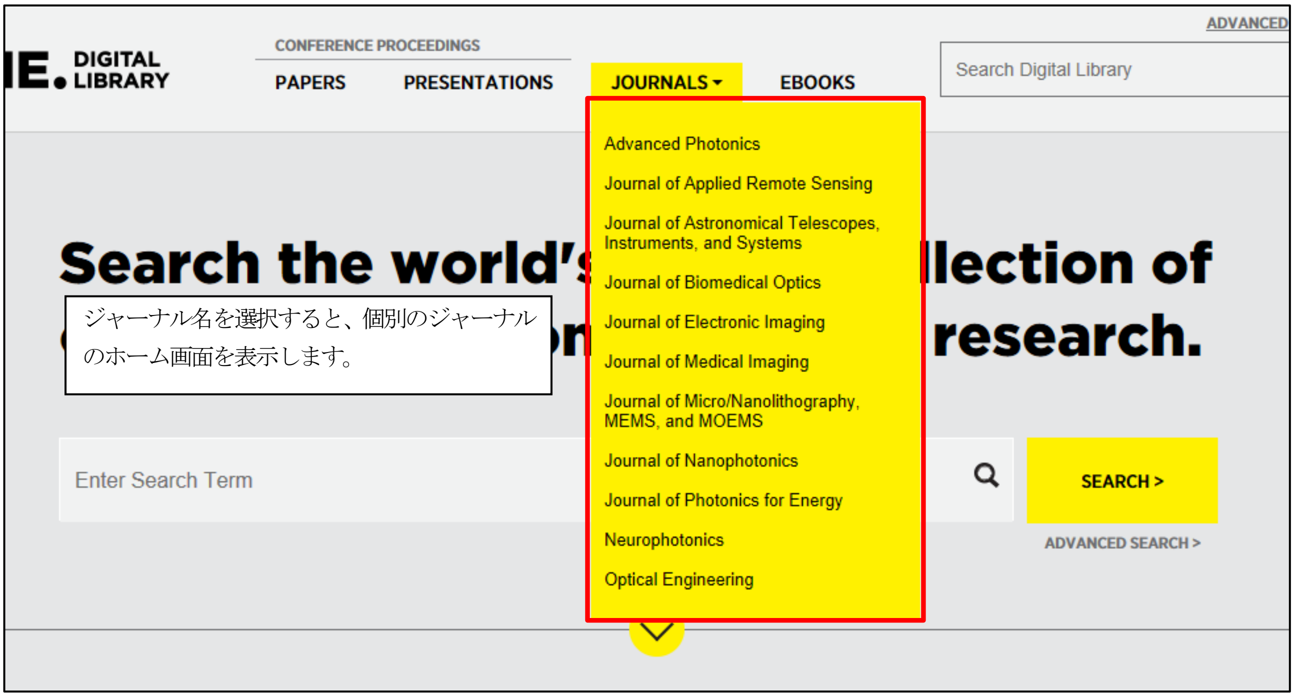

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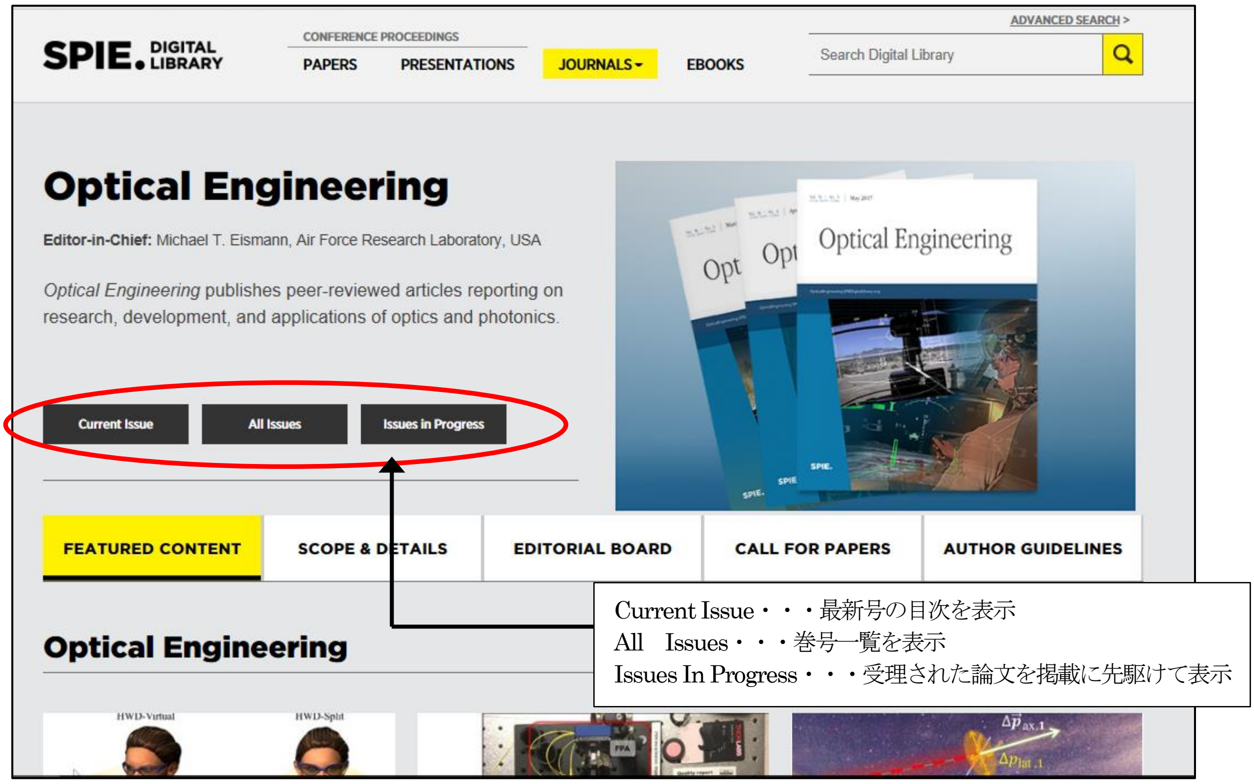

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Xiao-Cong (Larry) Yuan,
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NEWS AND COMMENTARIES

Perspectives on the future of photonics: the best is yet to come
Eugene Arthurs
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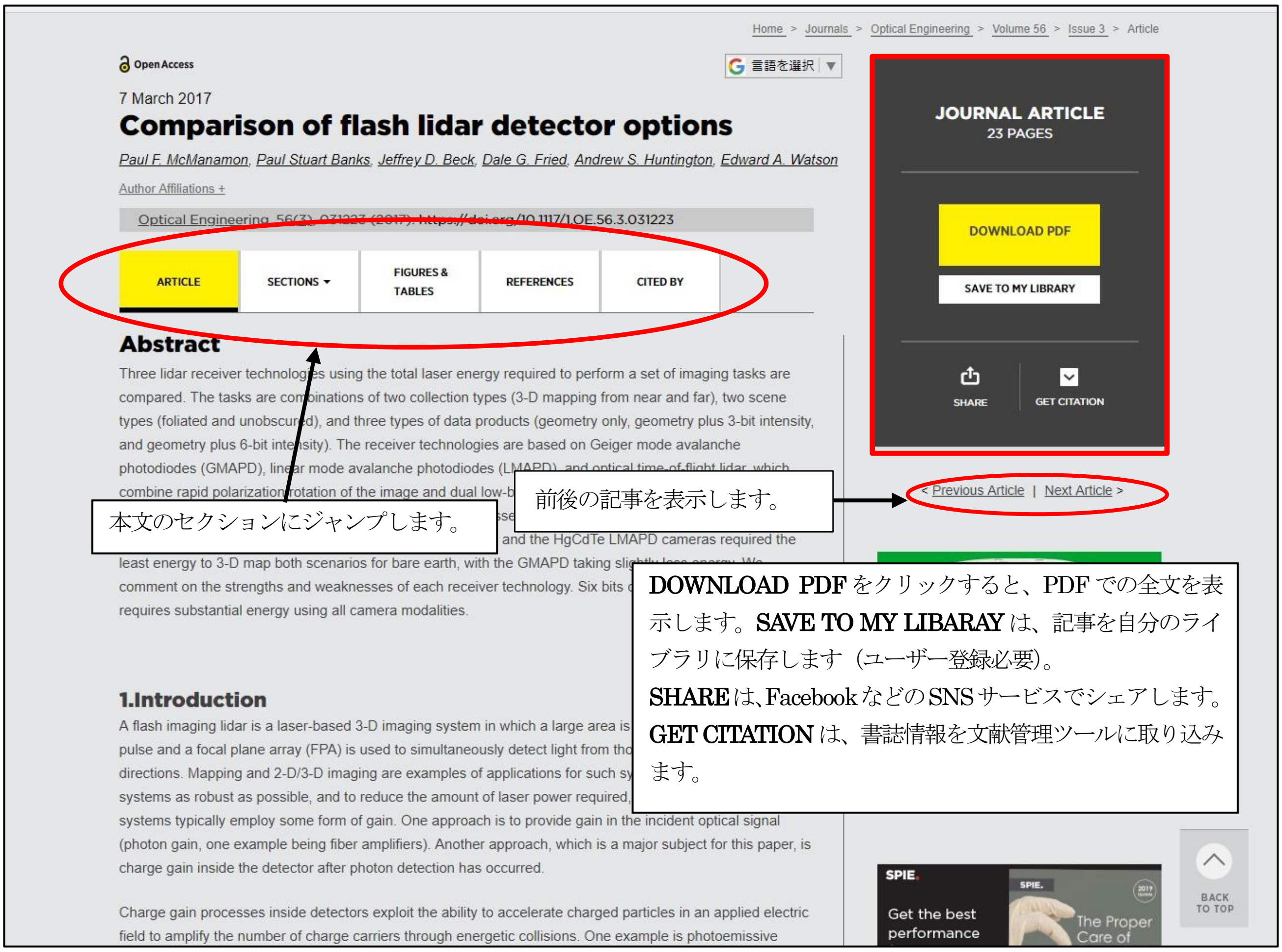

7 March 2017

Comparison of flash lidar detector options

Paul F. McManamon, Paul Stuart Banks, Jeffrey D. Beck, Dale G. Fried, Andrew S. Huntington, Edward A. Watson

Author Affiliations +

Optical Engineering, 56(3), 031223 (2017). https://doi.org/10.1117/1.OE.56.3.031223

Abstract

Three lidar receiver technologies using the total laser energy required to perform a set of imaging tasks are compared. The tasks are combinations of two collection types (3-D mapping from near and far), two scene types (foliated and unobscured), and three types of data products (geometry only, geometry plus 3-bit intensity, and geometry plus 6-bit intensity). The receiver technologies are based on Geiger mode avalanche photodiodes (GMAPD), linear mode avalanche photodiodes (LMAPD), and optical time-of-flight lidar, which combine rapid polarization rotation of the image and dual low-b

and the HgCdTe LMAPD cameras required the least energy to 3-D map both scenarios for bare earth, with the GMAPD taking sli

comment on the strengths and weaknesses of each receiver technology. Six bits

requires substantial energy using all camera modalities.

1.Introduction

A flash imaging lidar is a laser-based 3-D imaging system in which a large area is

pulse and a focal plane array (FPA) is used to simultaneously detect light from th

directions. Mapping and 2-D/3-D imaging are examples of applications for such sy

systems as robust as possible, and to reduce the amount of laser power required,

systems typically employ some form of gain. One approach is to provide gain in the incident optical signal (photon gain, one example being fiber amplifiers). Another approach, which is a major subject for this paper, is charge gain inside the detector after photon detection has occurred.

Charge gain processes inside detectors exploit the ability to accelerate charged particles in an applied electric field to amplify the number of charge carriers through energetic collisions. One example is photoemissive

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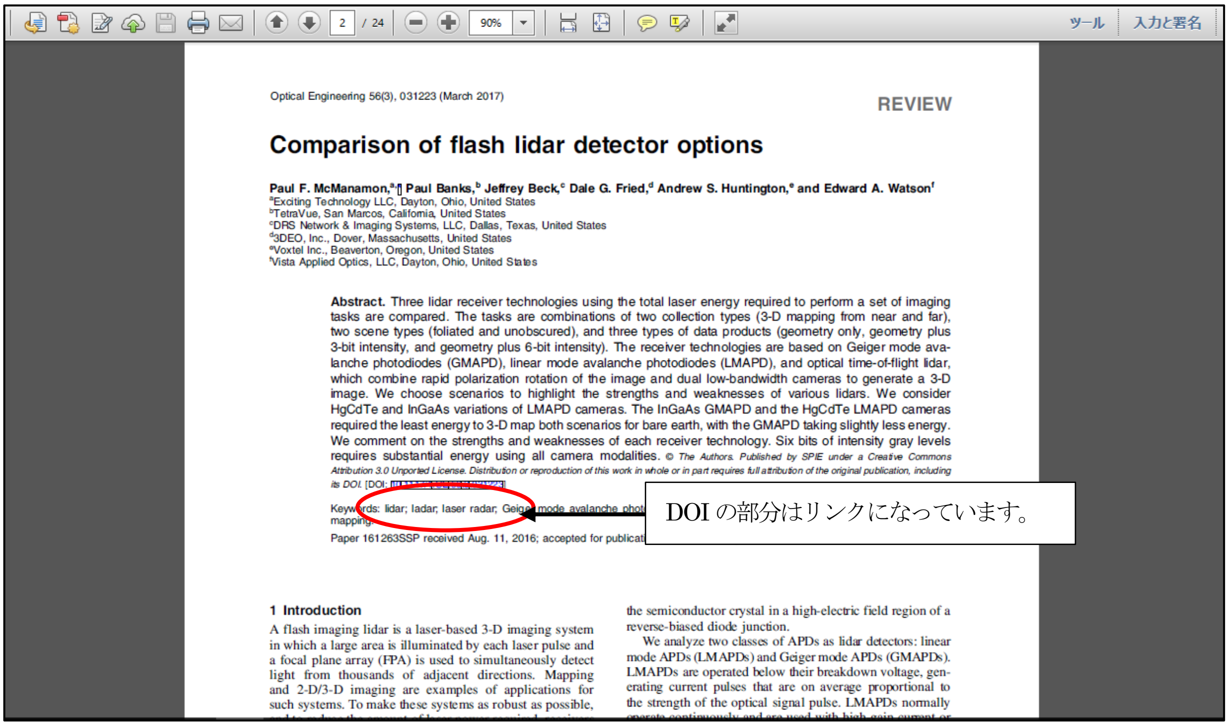

Optical Engineering 56(3), 031223 (March 2017)

REVIEW

Comparison of flash lidar detector options

Paul F. McManamon,[a] Paul Banks,[b] Jeffrey Beck,[c] Dale G. Fried,[d] Andrew S. Huntington,[e] and Edward A. Watson[f]
[a]Exciting Technology LLC, Dayton, Ohio, United States
[b]TetraVue, San Marcos, California, United States
[c]DRS Network & Imaging Systems, LLC, Dallas, Texas, United States
[d]3DEO, Inc., Dover, Massachusetts, United States
[e]Voxtel Inc., Beaverton, Oregon, United States
[f]Vista Applied Optics, LLC, Dayton, Ohio, United States

Abstract. Three lidar receiver technologies using the total laser energy required to perform a set of imaging tasks are compared. The tasks are combinations of two collection types (3-D mapping from near and far), two scene types (foliated and unobscured), and three types of data products (geometry only, geometry plus 3-bit intensity, and geometry plus 6-bit intensity). The receiver technologies are based on Geiger mode avalanche photodiodes (GMAPD), linear mode avalanche photodiodes (LMAPD), and optical time-of-flight lidar, which combine rapid polarization rotation of the image and dual low-bandwidth cameras to generate a 3-D image. We choose scenarios to highlight the strengths and weaknesses of various lidars. We consider HgCdTe and InGaAs variations of LMAPD cameras. The InGaAs GMAPD and the HgCdTe LMAPD cameras required the least energy to 3-D map both scenarios for bare earth, with the GMAPD taking slightly less energy. We comment on the strengths and weaknesses of each receiver technology. Six bits of intensity gray levels requires substantial energy using all camera modalities. *© The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI.* [DOI: [illegible]]

Keywords: lidar; ladar; laser radar; Geiger mode avalanche phot mapping.

Paper 161263SSP received Aug. 11, 2016; accepted for publicat

1 Introduction

A flash imaging lidar is a laser-based 3-D imaging system in which a large area is illuminated by each laser pulse and a focal plane array (FPA) is used to simultaneously detect light from thousands of adjacent directions. Mapping and 2-D/3-D imaging are examples of applications for such systems. To make these systems as robust as possible,

the semiconductor crystal in a high-electric field region of a reverse-biased diode junction.

We analyze two classes of APDs as lidar detectors: linear mode APDs (LMAPDs) and Geiger mode APDs (GMAPDs). LMAPDs are operated below their breakdown voltage, generating current pulses that are on average proportional to the strength of the optical signal pulse. LMAPDs normally

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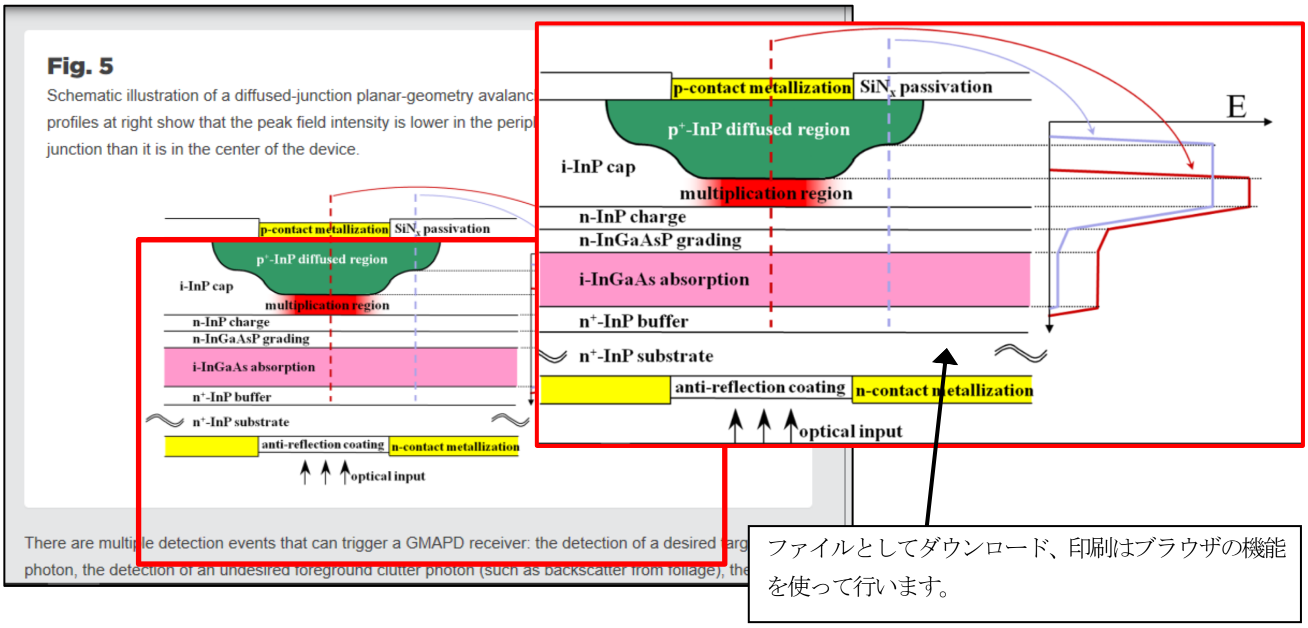

Fig. 5

Schematic illustration of a diffused-junction planar-geometry avalanc
profiles at right show that the peak field intensity is lower in the peripl
junction than it is in the center of the device.

There are multiple detection events that can trigger a GMAPD receiver: the detection of a desired targ
photon, the detection of an undesired foreground clutter photon (such as backscatter from foliage), the

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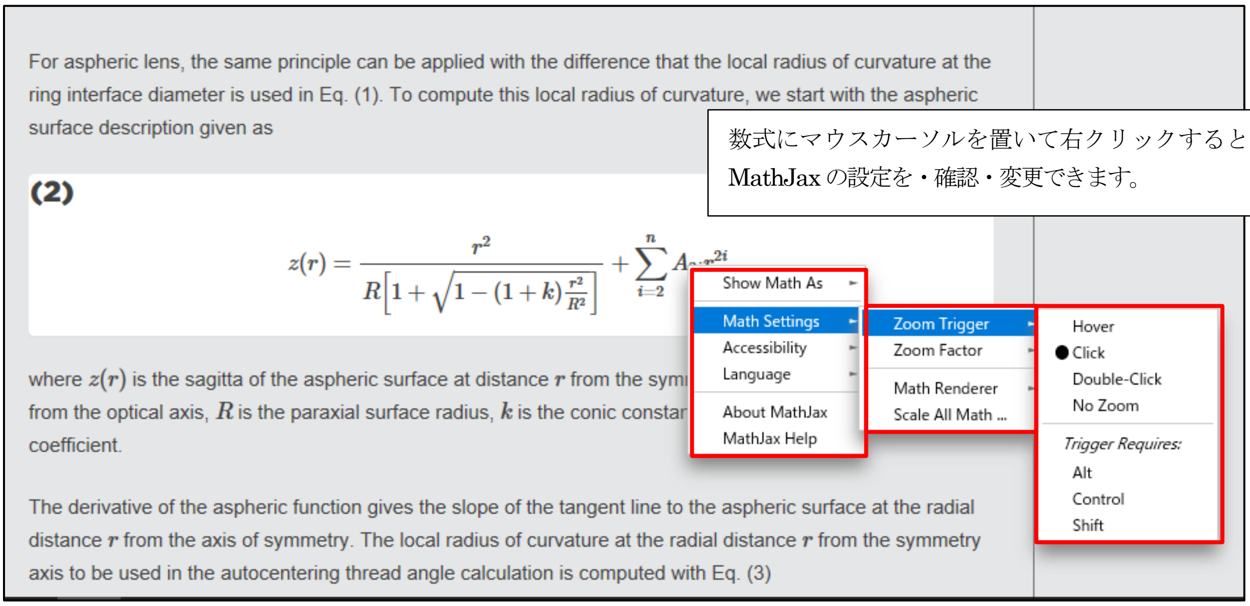

For aspheric lens, the same principle can be applied with the difference that the local radius of curvature at the ring interface diameter is used in Eq. (1). To compute this local radius of curvature, we start with the aspheric surface description given as

(2)

$$z(r)=\frac{r^2}{R\left[1+\sqrt{1-(1+k)\frac{r^2}{R^2}}\right]}+\sum_{i=2}^{n}A_{2i}r^{2i}$$

where $z(r)$ is the sagitta of the aspheric surface at distance r from the symm
from the optical axis, R is the paraxial surface radius, k is the conic constar
coefficient.

The derivative of the aspheric function gives the slope of the tangent line to the aspheric surface at the radial distance r from the axis of symmetry. The local radius of curvature at the radial distance r from the symmetry axis to be used in the autocentering thread angle calculation is computed with Eq. (3)

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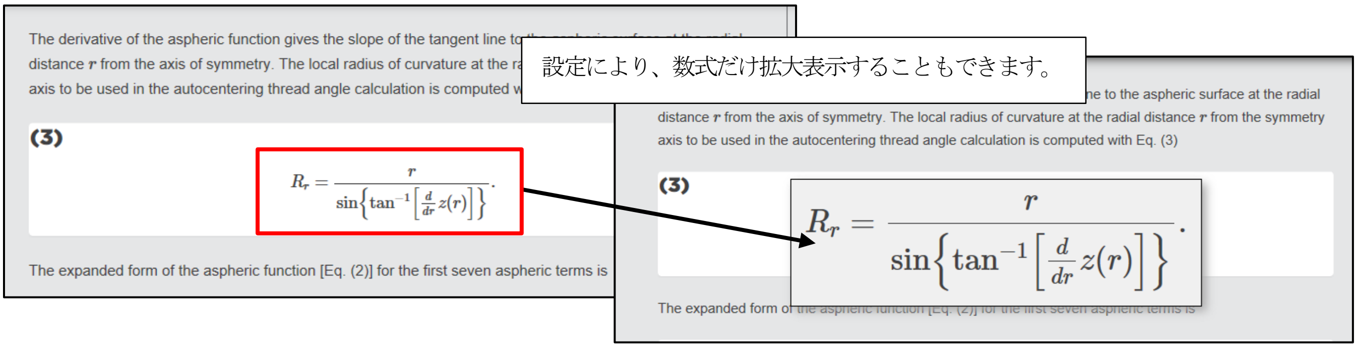

The derivative of the aspheric function gives the slope of the tangent line to the aspheric surface at the radial distance r from the axis of symmetry. The local radius of curvature at the radial distance r from the symmetry axis to be used in the autocentering thread angle calculation is computed with Eq. (3)

(3)

$$R_r=\frac{r}{\sin\left\{\tan^{-1}\left[\frac{d}{dr}z(r)\right]\right\}}.$$

The expanded form of the aspheric function [Eq. (2)] for the first seven aspheric terms is

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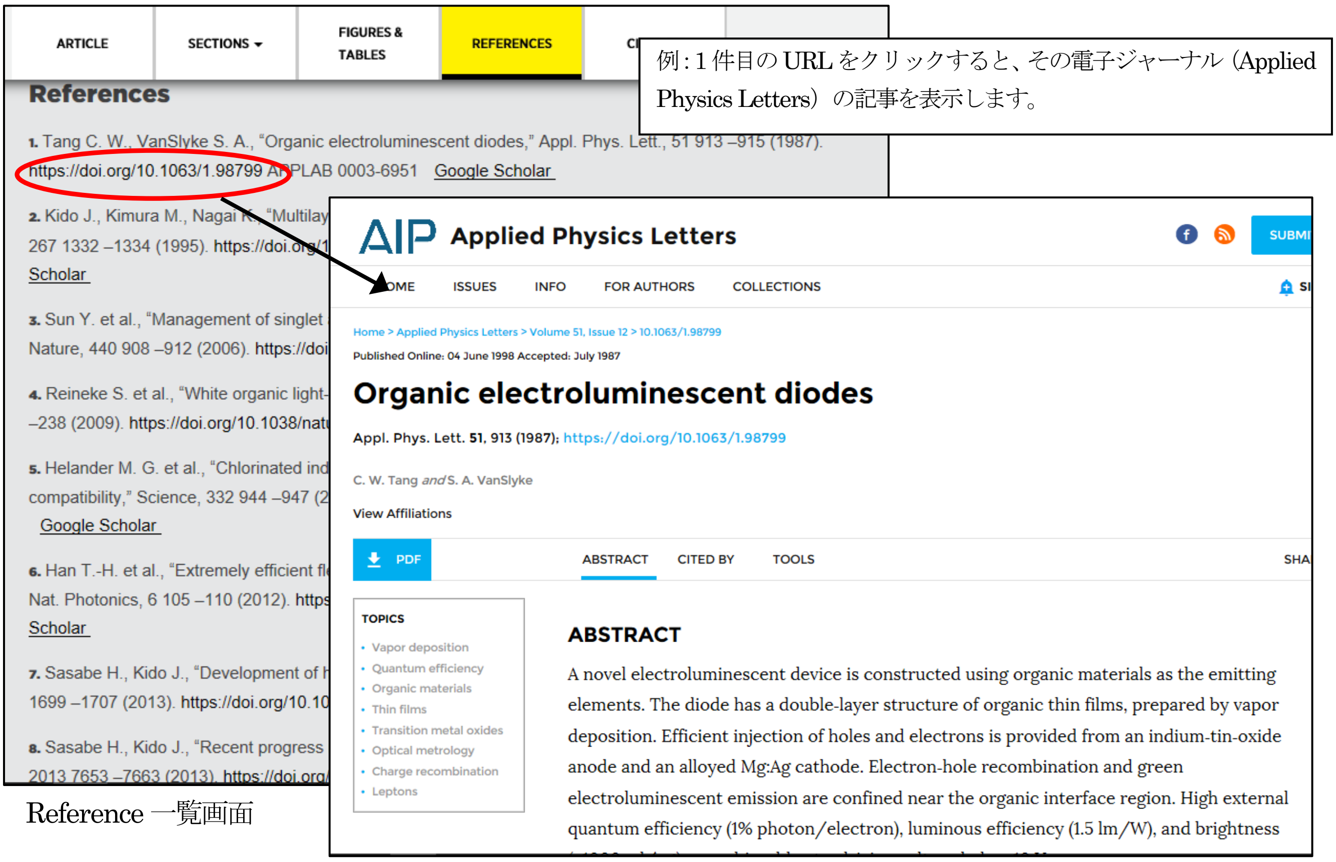

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Published Online: 04 June 1998 Accepted: July 1987

Organic electroluminescent diodes

Appl. Phys. Lett. 51, 913 (1987); https://doi.org/10.1063/1.98799

C. W. Tang *and* S. A. VanSlyke

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TOPICS
- Vapor deposition
- Quantum efficiency
- Organic materials
- Thin films
- Transition metal oxides
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ABSTRACT

A novel electroluminescent device is constructed using organic materials as the emitting elements. The diode has a double-layer structure of organic thin films, prepared by vapor deposition. Efficient injection of holes and electrons is provided from an indium-tin-oxide anode and an alloyed Mg:Ag cathode. Electron-hole recombination and green electroluminescent emission are confined near the organic interface region. High external quantum efficiency (1% photon/electron), luminous efficiency (1.5 lm/W), and brightness

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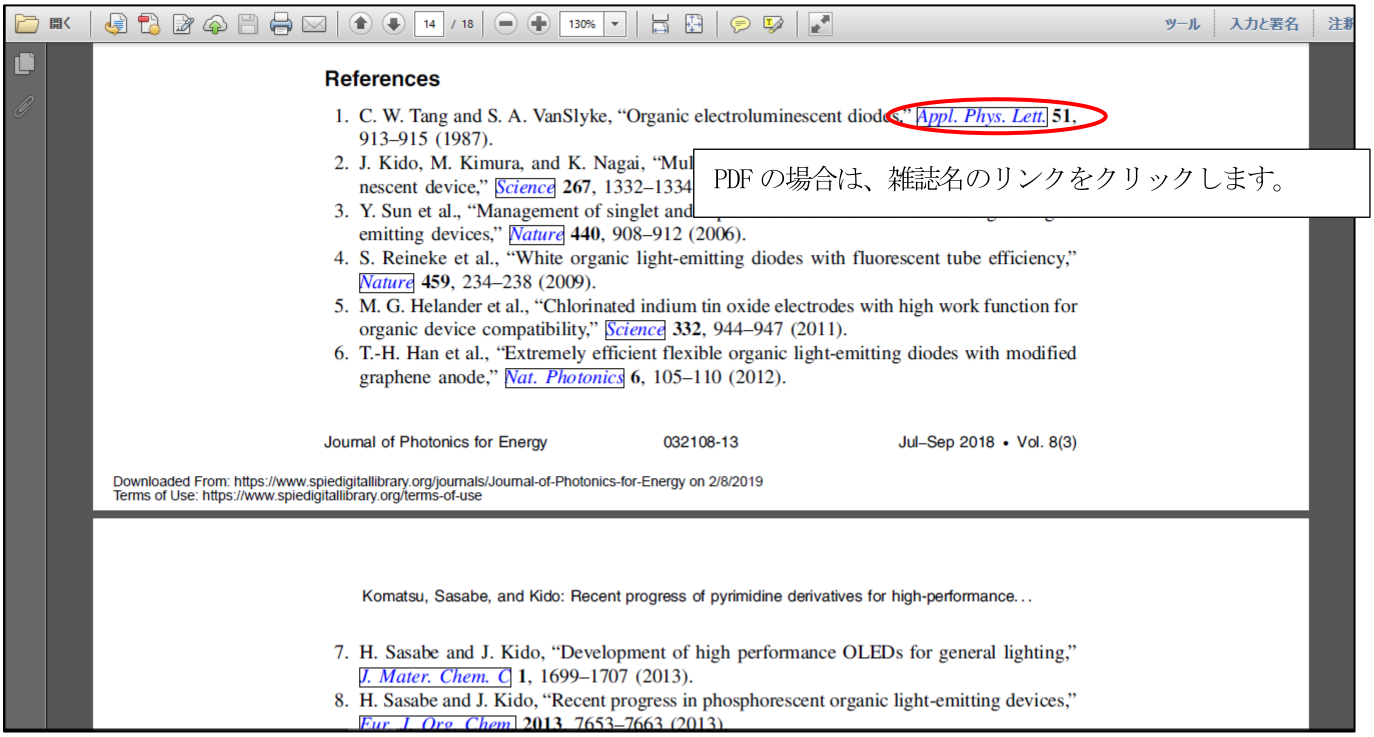

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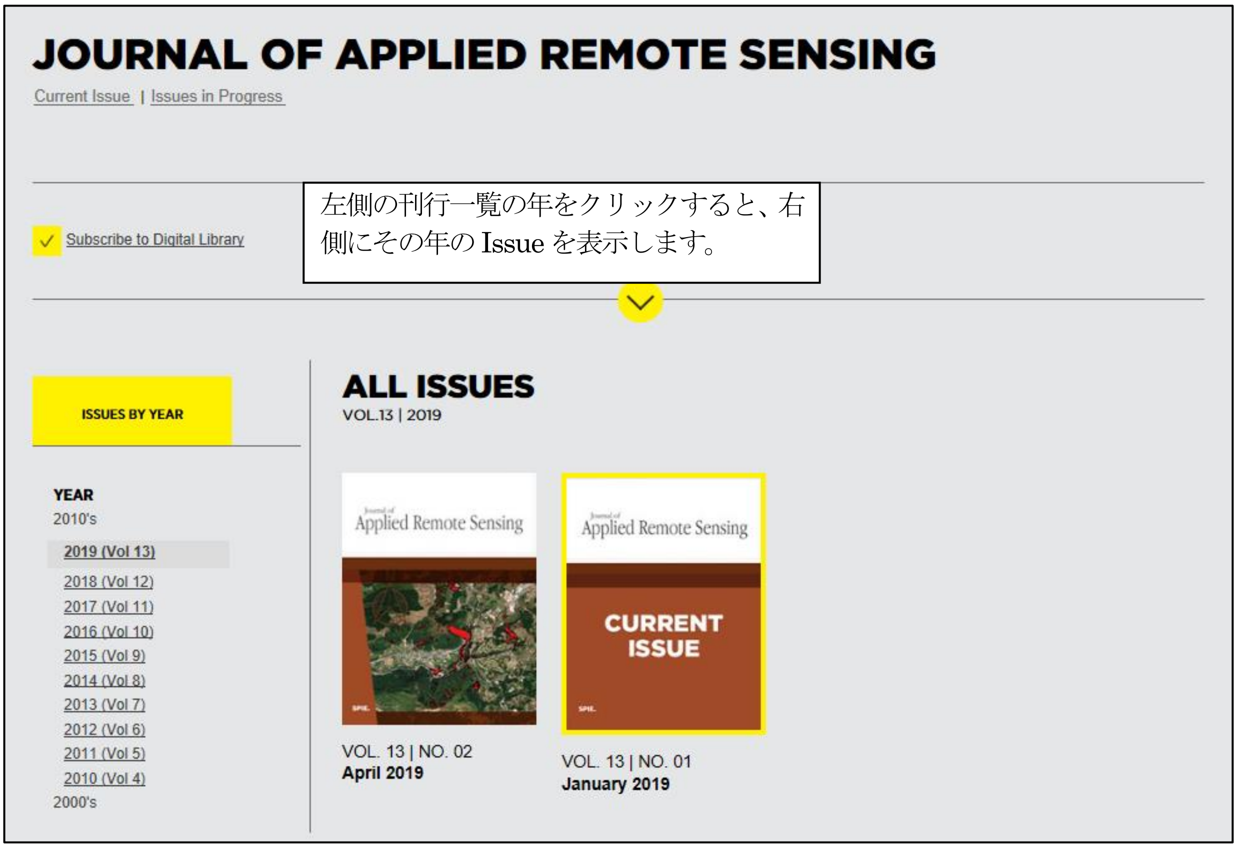

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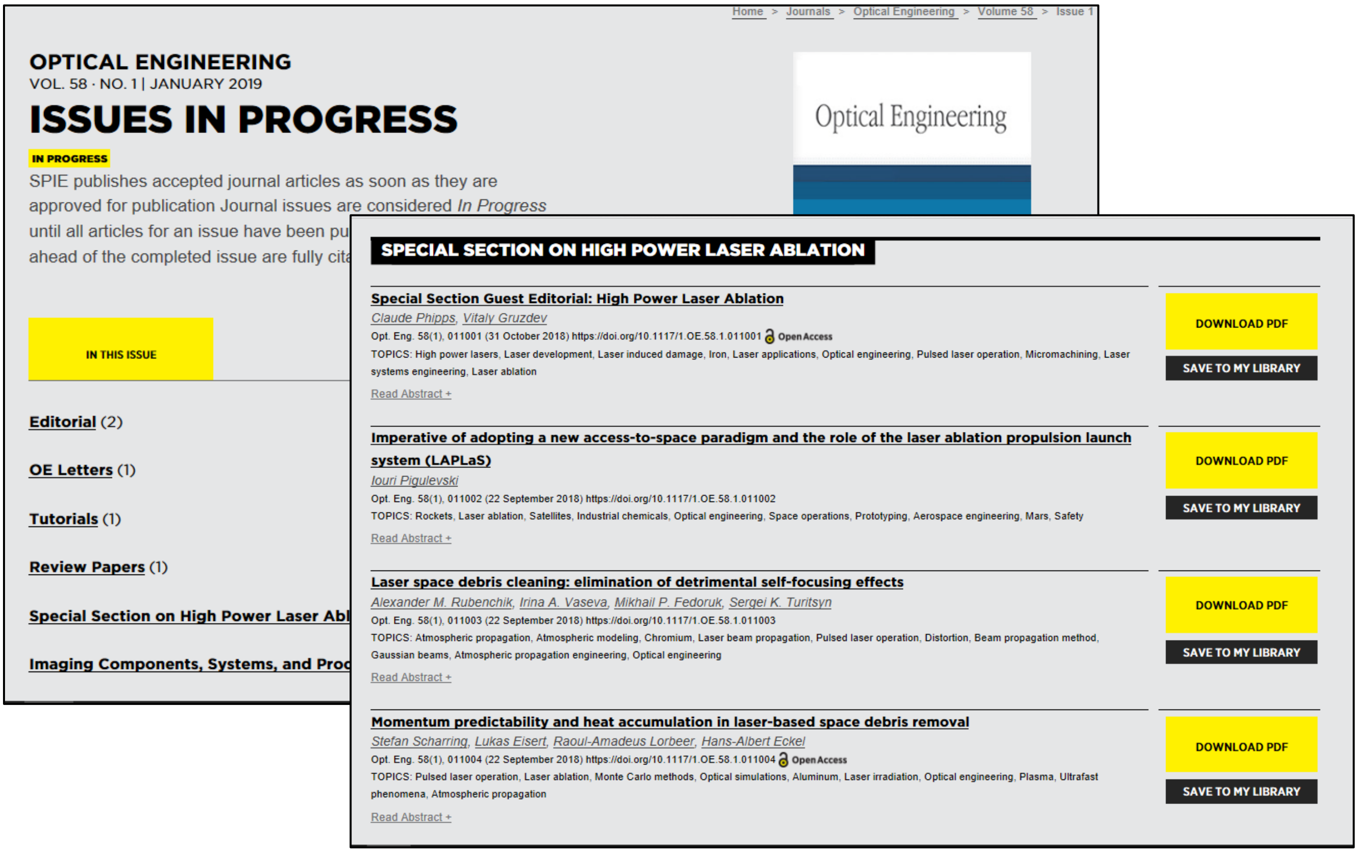

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Iouri Pigulevski
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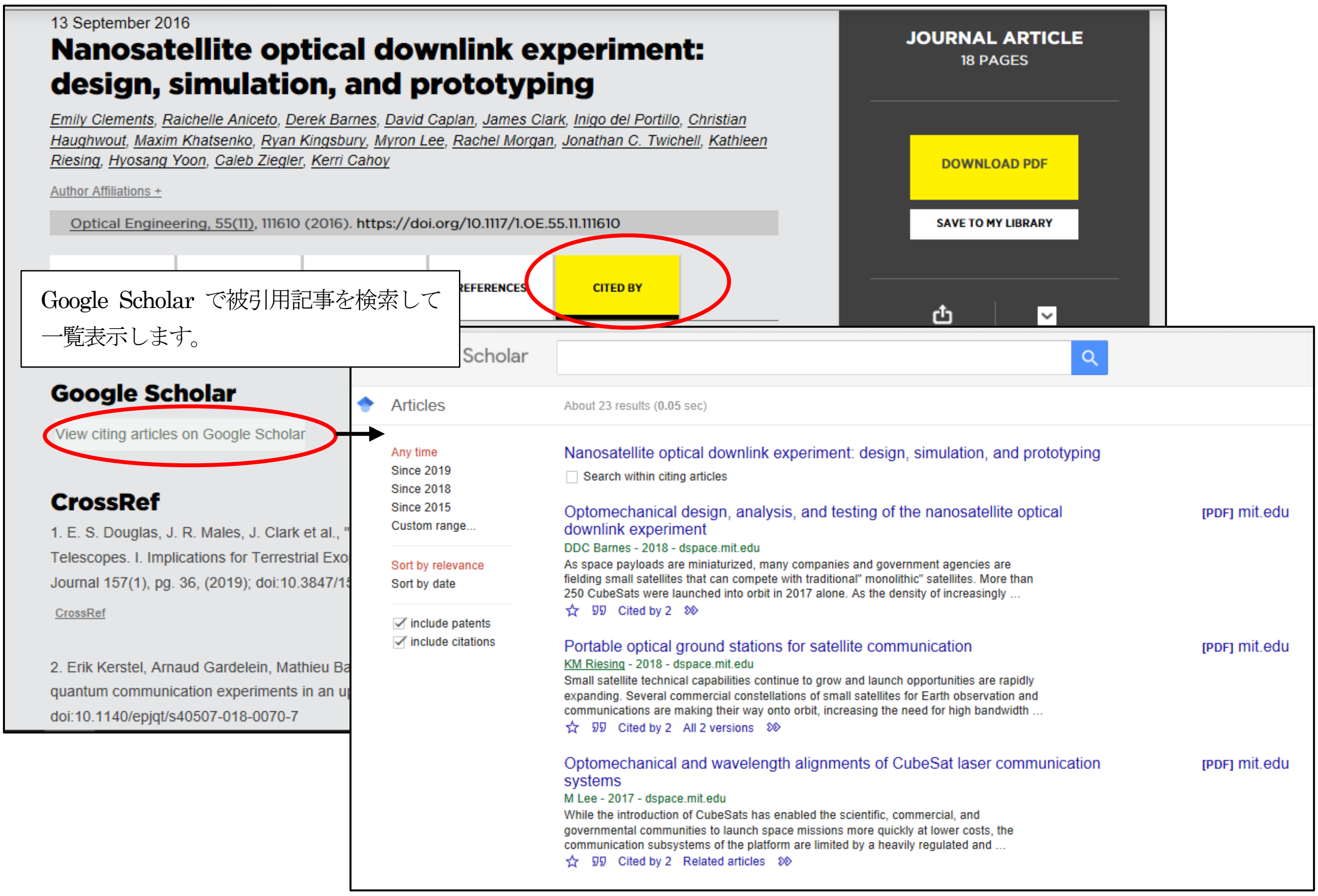

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Emily Clements, Raichelle Aniceto, Derek Barnes, David Caplan, James Clark, Inigo del Portillo, Christian Haughwout, Maxim Khatsenko, Ryan Kingsbury, Myron Lee, Rachel Morgan, Jonathan C. Twichell, Kathleen Riesing, Hyosang Yoon, Caleb Ziegler, Kerri Cahoy

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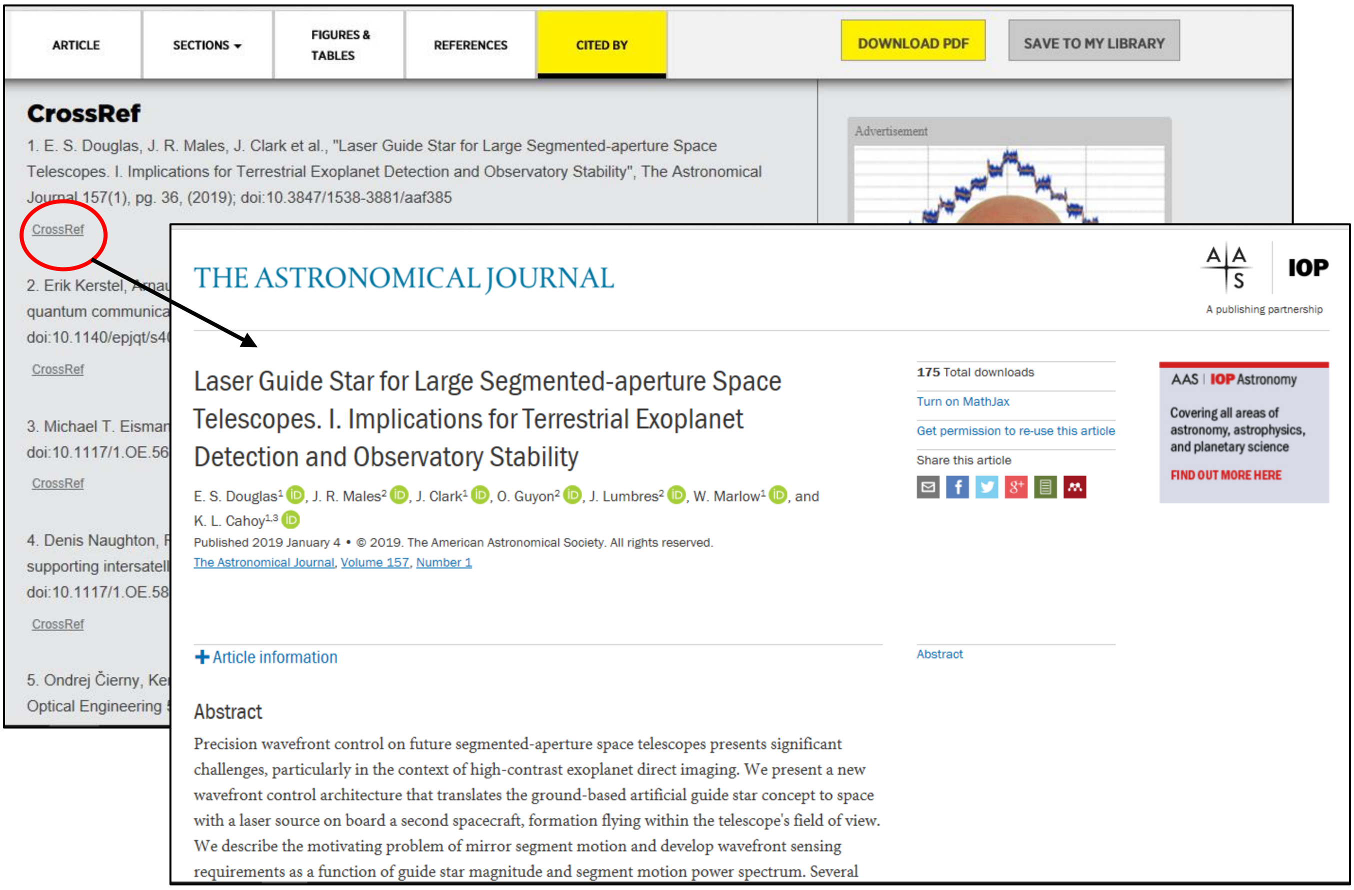

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THE ASTRONOMICAL JOURNAL

Laser Guide Star for Large Segmented-aperture Space Telescopes. I. Implications for Terrestrial Exoplanet Detection and Observatory Stability

E. S. Douglas[1], J. R. Males[2], J. Clark[1], O. Guyon[2], J. Lumbres[2], W. Marlow[1], and K. L. Cahoy[1,3]

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The Astronomical Journal, Volume 157, Number 1

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Abstract

Abstract

Precision wavefront control on future segmented-aperture space telescopes presents significant challenges, particularly in the context of high-contrast exoplanet direct imaging. We present a new wavefront control architecture that translates the ground-based artificial guide star concept to space with a laser source on board a second spacecraft, formation flying within the telescope's field of view. We describe the motivating problem of mirror segment motion and develop wavefront sensing requirements as a function of guide star magnitude and segment motion power spectrum. Several

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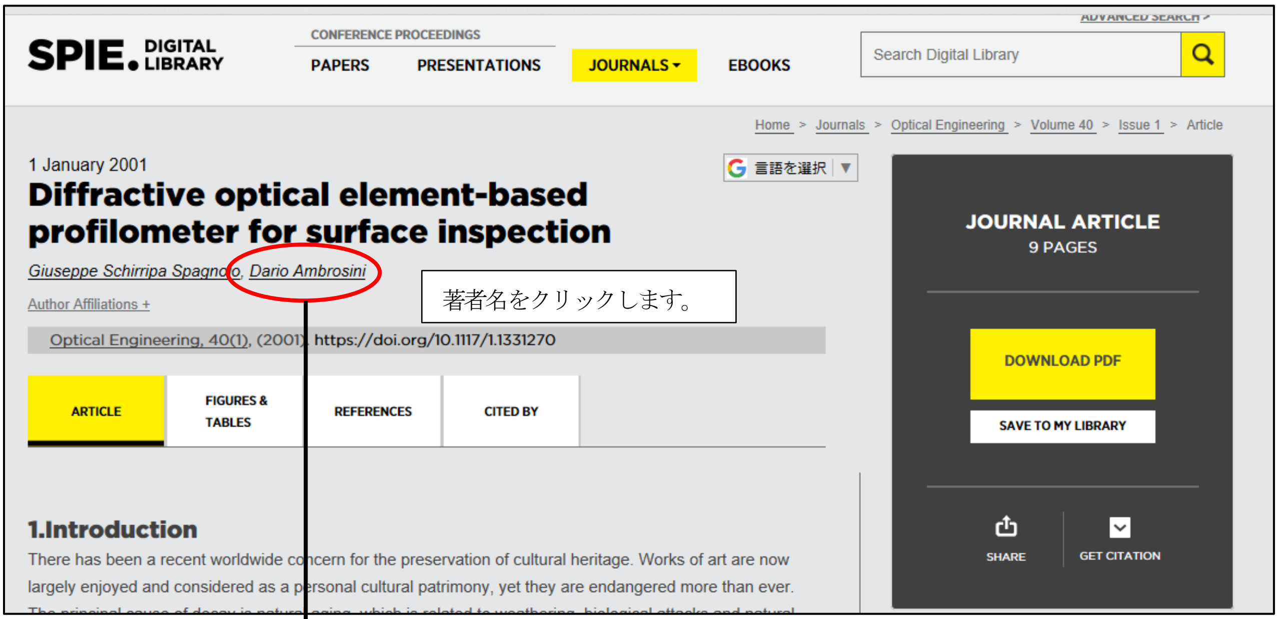

1 January 2001

Diffractive optical element-based profilometer for surface inspection

Giuseppe Schirripa Spagnolo, Dario Ambrosini

Author Affiliations +

Optical Engineering, 40(1), (2001). https://doi.org/10.1117/1.1331270

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1.Introduction

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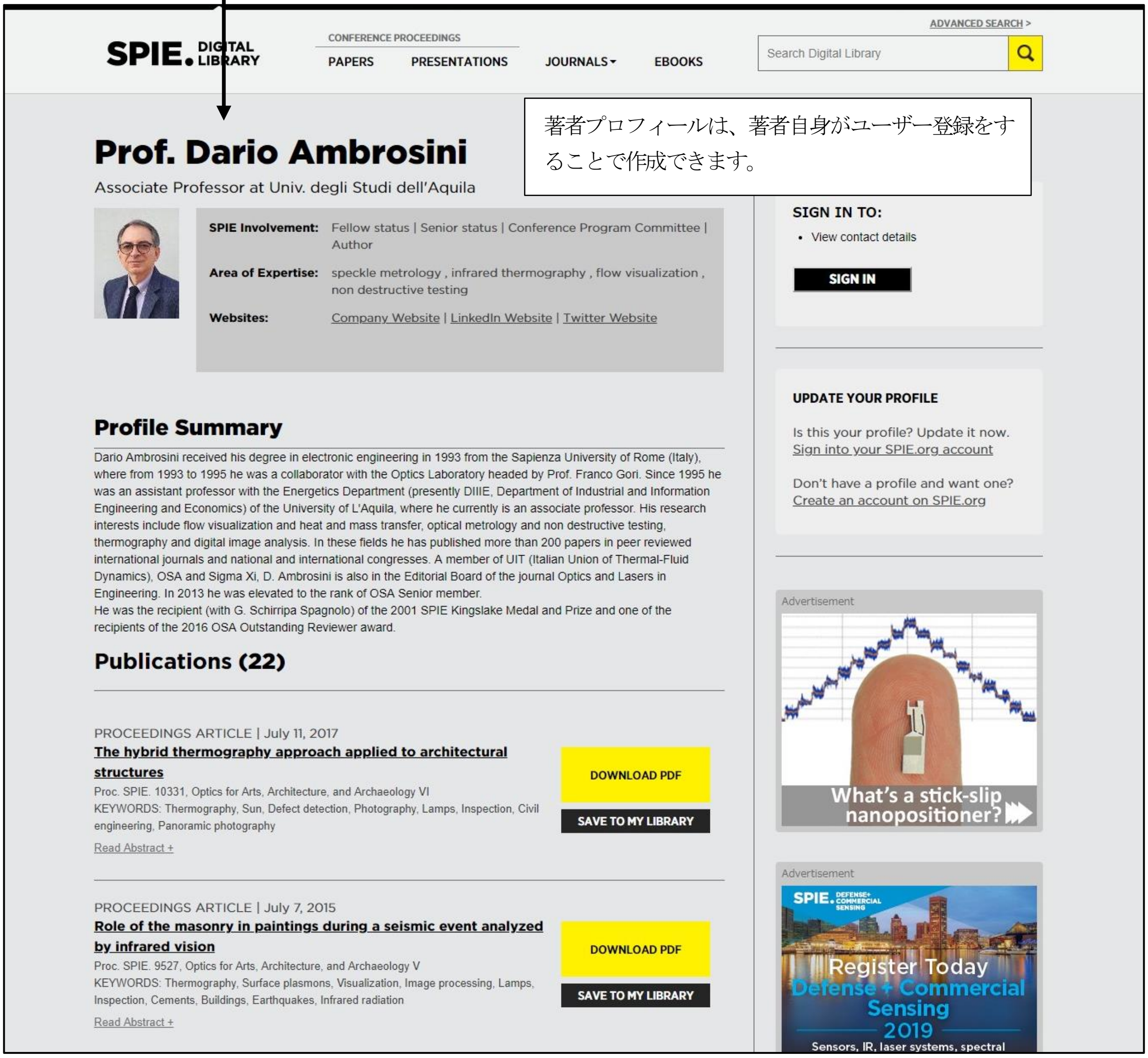

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Prof. Dario Ambrosini

Associate Professor at Univ. degli Studi dell'Aquila

SPIE Involvement: Fellow status | Senior status | Conference Program Committee | Author

Area of Expertise: speckle metrology , infrared thermography , flow visualization , non destructive testing

Websites: Company Website | LinkedIn Website | Twitter Website

Profile Summary

Dario Ambrosini received his degree in electronic engineering in 1993 from the Sapienza University of Rome (Italy), where from 1993 to 1995 he was a collaborator with the Optics Laboratory headed by Prof. Franco Gori. Since 1995 he was an assistant professor with the Energetics Department (presently DIIIE, Department of Industrial and Information Engineering and Economics) of the University of L'Aquila, where he currently is an associate professor. His research interests include flow visualization and heat and mass transfer, optical metrology and non destructive testing, thermography and digital image analysis. In these fields he has published more than 200 papers in peer reviewed international journals and national and international congresses. A member of UIT (Italian Union of Thermal-Fluid Dynamics), OSA and Sigma Xi, D. Ambrosini is also in the Editorial Board of the journal Optics and Lasers in Engineering. In 2013 he was elevated to the rank of OSA Senior member.
He was the recipient (with G. Schirripa Spagnolo) of the 2001 SPIE Kingslake Medal and Prize and one of the recipients of the 2016 OSA Outstanding Reviewer award.

Publications (22)

PROCEEDINGS ARTICLE | July 11, 2017
The hybrid thermography approach applied to architectural structures
Proc. SPIE. 10331, Optics for Arts, Architecture, and Archaeology VI
KEYWORDS: Thermography, Sun, Defect detection, Photography, Lamps, Inspection, Civil engineering, Panoramic photography
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Role of the masonry in paintings during a seismic event analyzed by infrared vision
Proc. SPIE. 9527, Optics for Arts, Architecture, and Archaeology V
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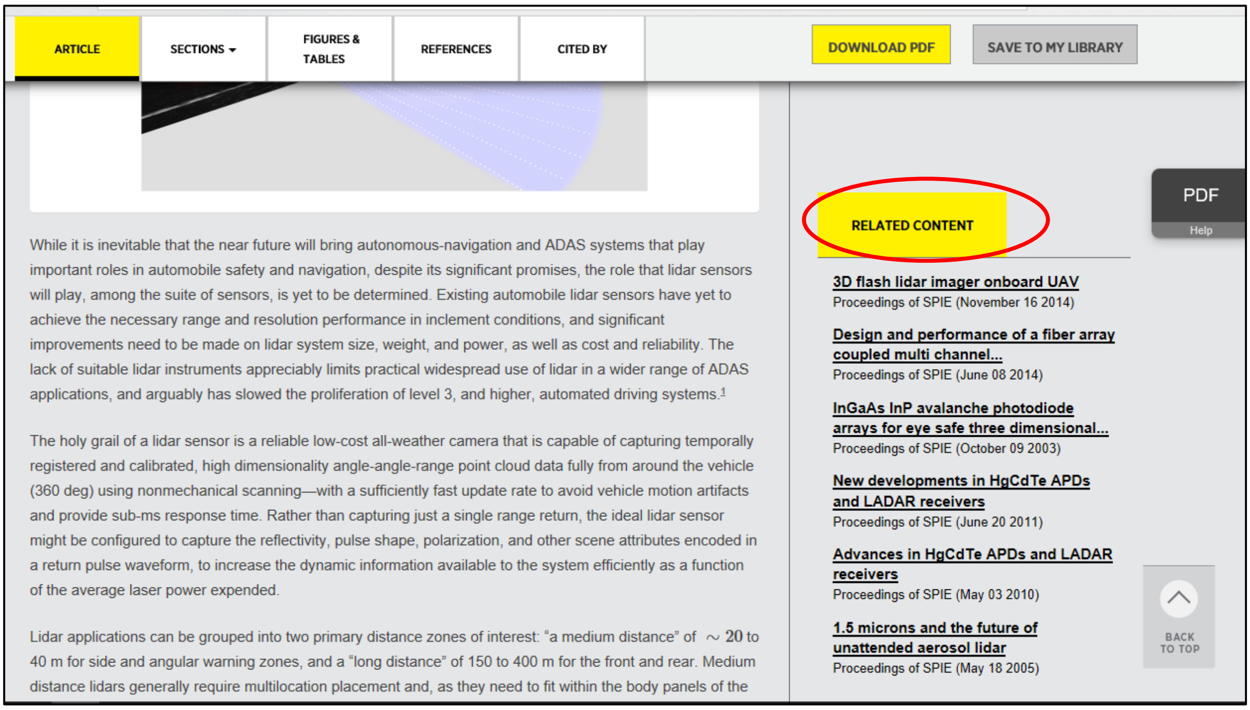

While it is inevitable that the near future will bring autonomous-navigation and ADAS systems that play important roles in automobile safety and navigation, despite its significant promises, the role that lidar sensors will play, among the suite of sensors, is yet to be determined. Existing automobile lidar sensors have yet to achieve the necessary range and resolution performance in inclement conditions, and significant improvements need to be made on lidar system size, weight, and power, as well as cost and reliability. The lack of suitable lidar instruments appreciably limits practical widespread use of lidar in a wider range of ADAS applications, and arguably has slowed the proliferation of level 3, and higher, automated driving systems.[1]

The holy grail of a lidar sensor is a reliable low-cost all-weather camera that is capable of capturing temporally registered and calibrated, high dimensionality angle-angle-range point cloud data fully from around the vehicle (360 deg) using nonmechanical scanning—with a sufficiently fast update rate to avoid vehicle motion artifacts and provide sub-ms response time. Rather than capturing just a single range return, the ideal lidar sensor might be configured to capture the reflectivity, pulse shape, polarization, and other scene attributes encoded in a return pulse waveform, to increase the dynamic information available to the system efficiently as a function of the average laser power expended.

Lidar applications can be grouped into two primary distance zones of interest: “a medium distance” of ∼20 to 40 m for side and angular warning zones, and a “long distance” of 150 to 400 m for the front and rear. Medium distance lidars generally require multilocation placement and, as they need to fit within the body panels of the

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Proceedings of SPIE (June 20 2011)

Advances in HgCdTe APDs and LADAR receivers
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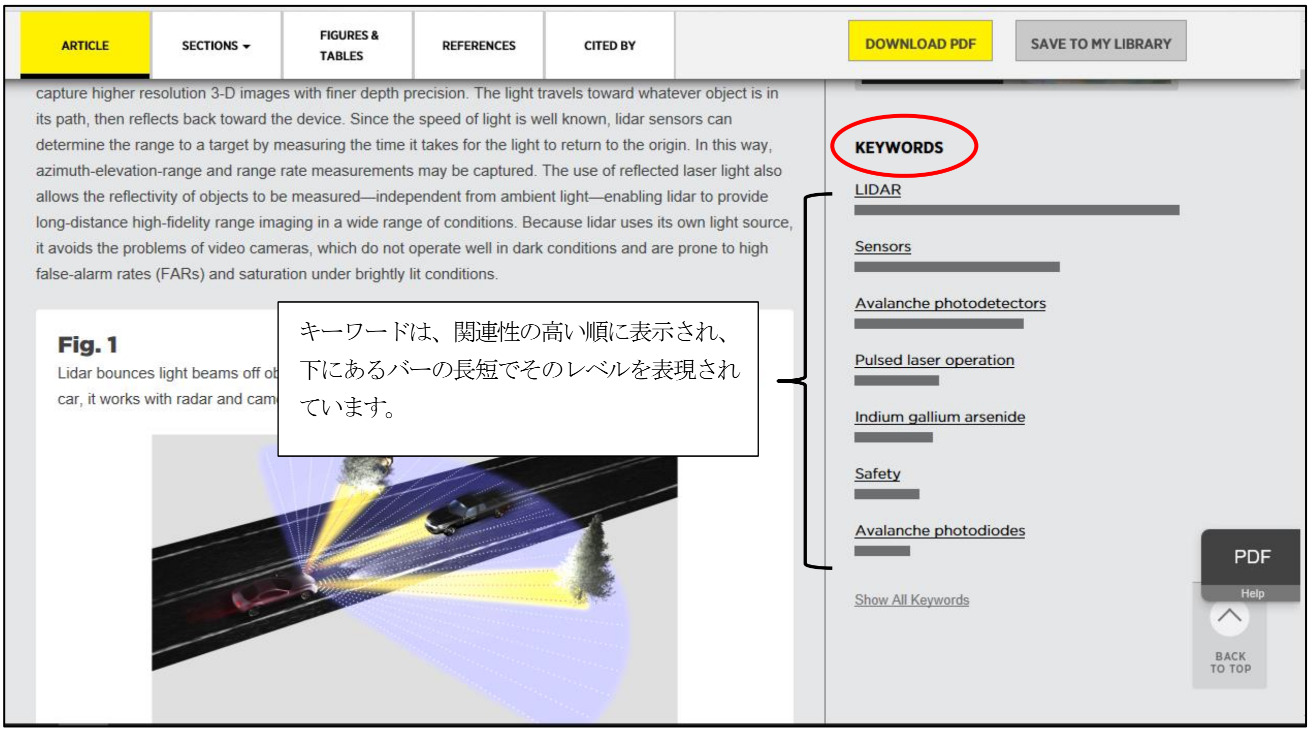

capture higher resolution 3-D images with finer depth precision. The light travels toward whatever object is in its path, then reflects back toward the device. Since the speed of light is well known, lidar sensors can determine the range to a target by measuring the time it takes for the light to return to the origin. In this way, azimuth-elevation-range and range rate measurements may be captured. The use of reflected laser light also allows the reflectivity of objects to be measured—independent from ambient light—enabling lidar to provide long-distance high-fidelity range imaging in a wide range of conditions. Because lidar uses its own light source, it avoids the problems of video cameras, which do not operate well in dark conditions and are prone to high false-alarm rates (FARs) and saturation under brightly lit conditions.

Fig. 1
Lidar bounces light beams off ob
car, it works with radar and cam

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- LIDAR
- Sensors
- Avalanche photodetectors
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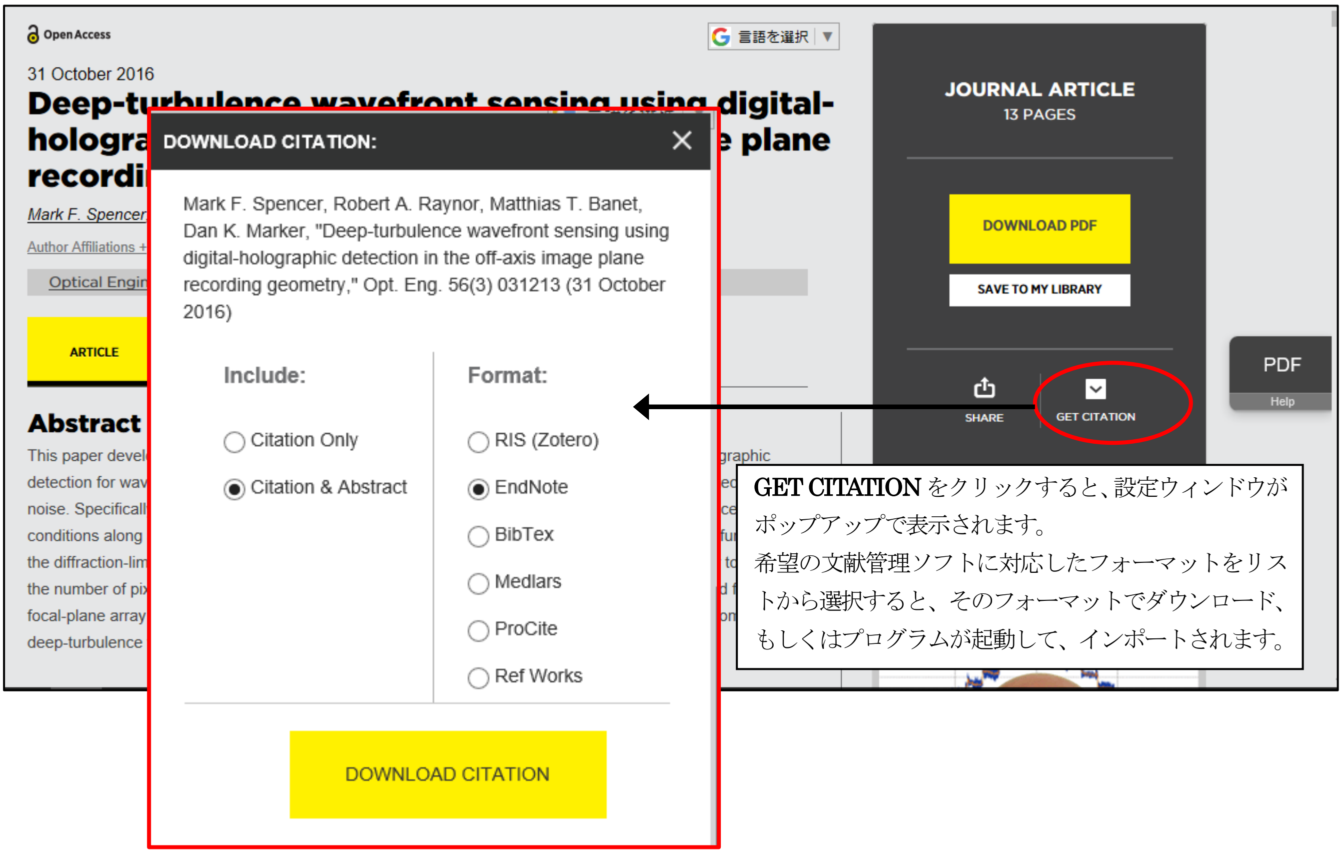

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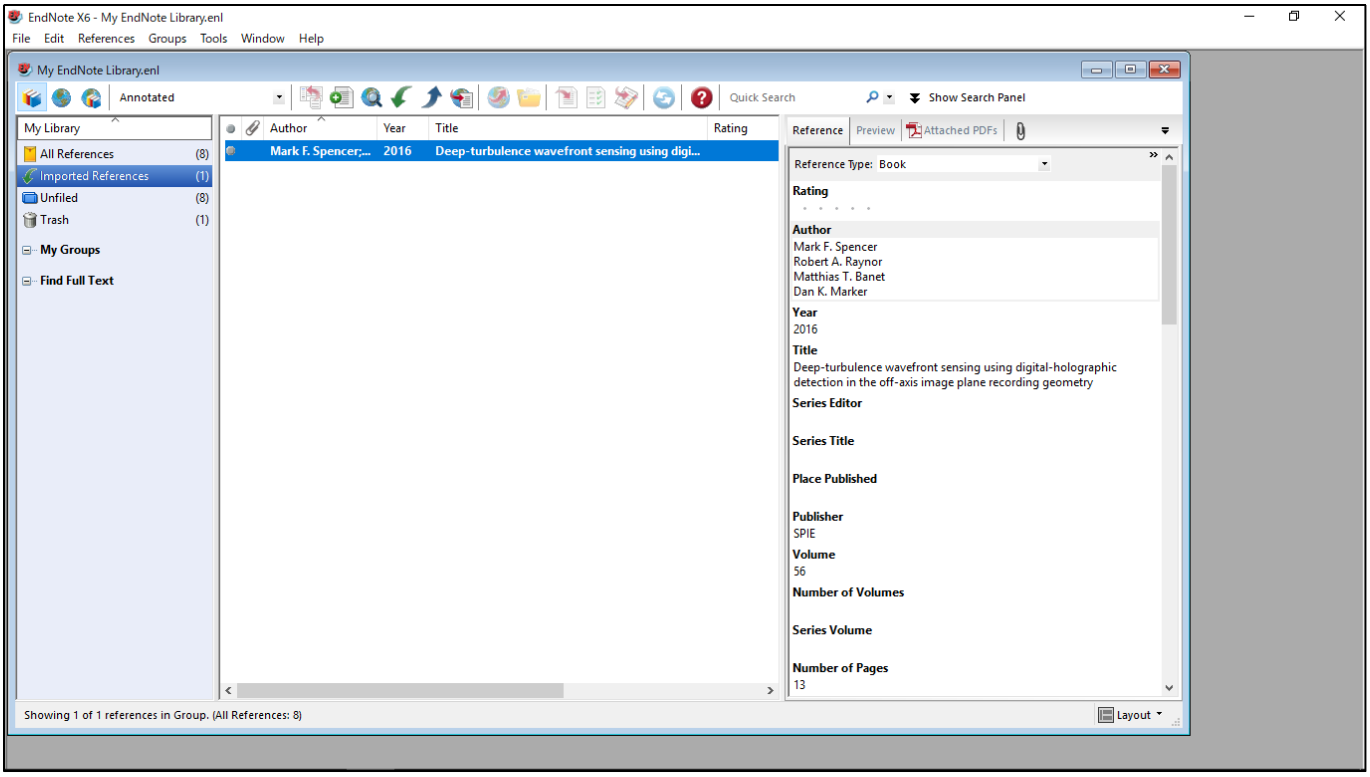

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Year
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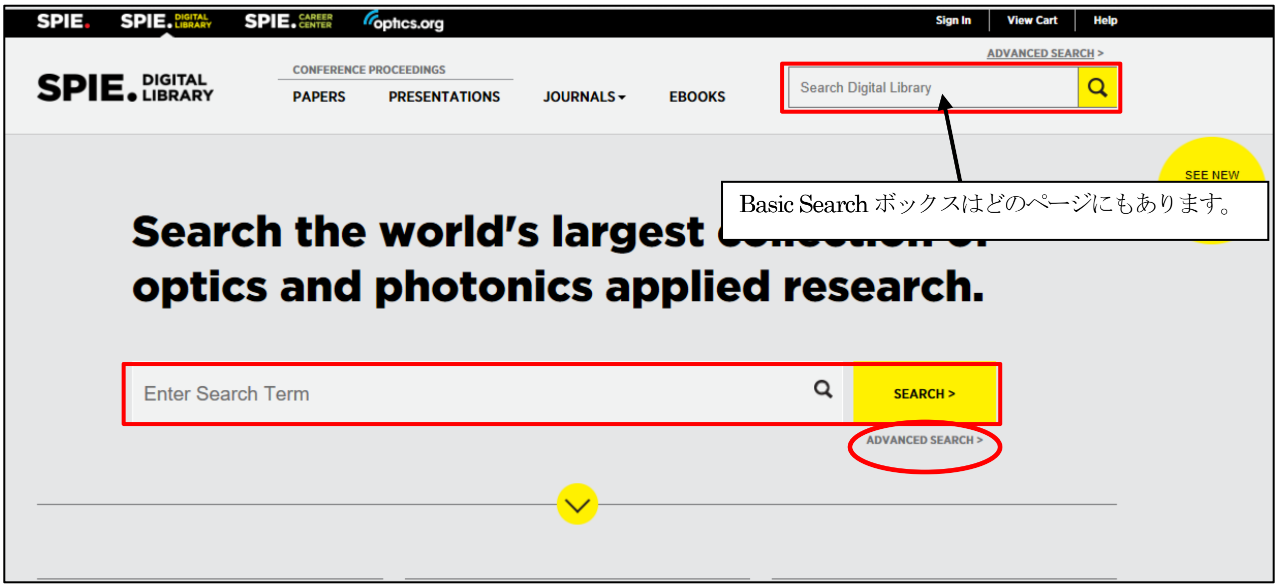

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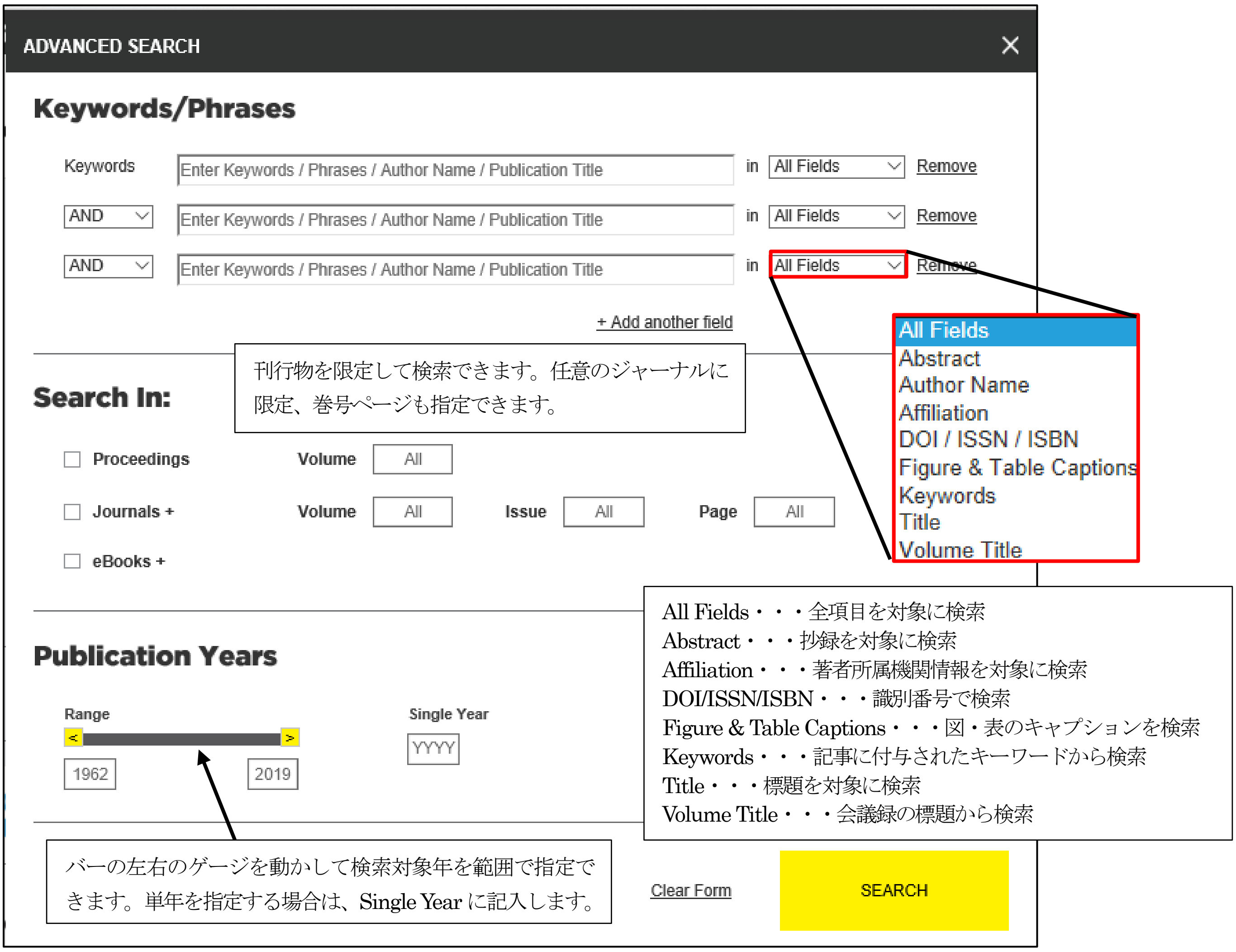

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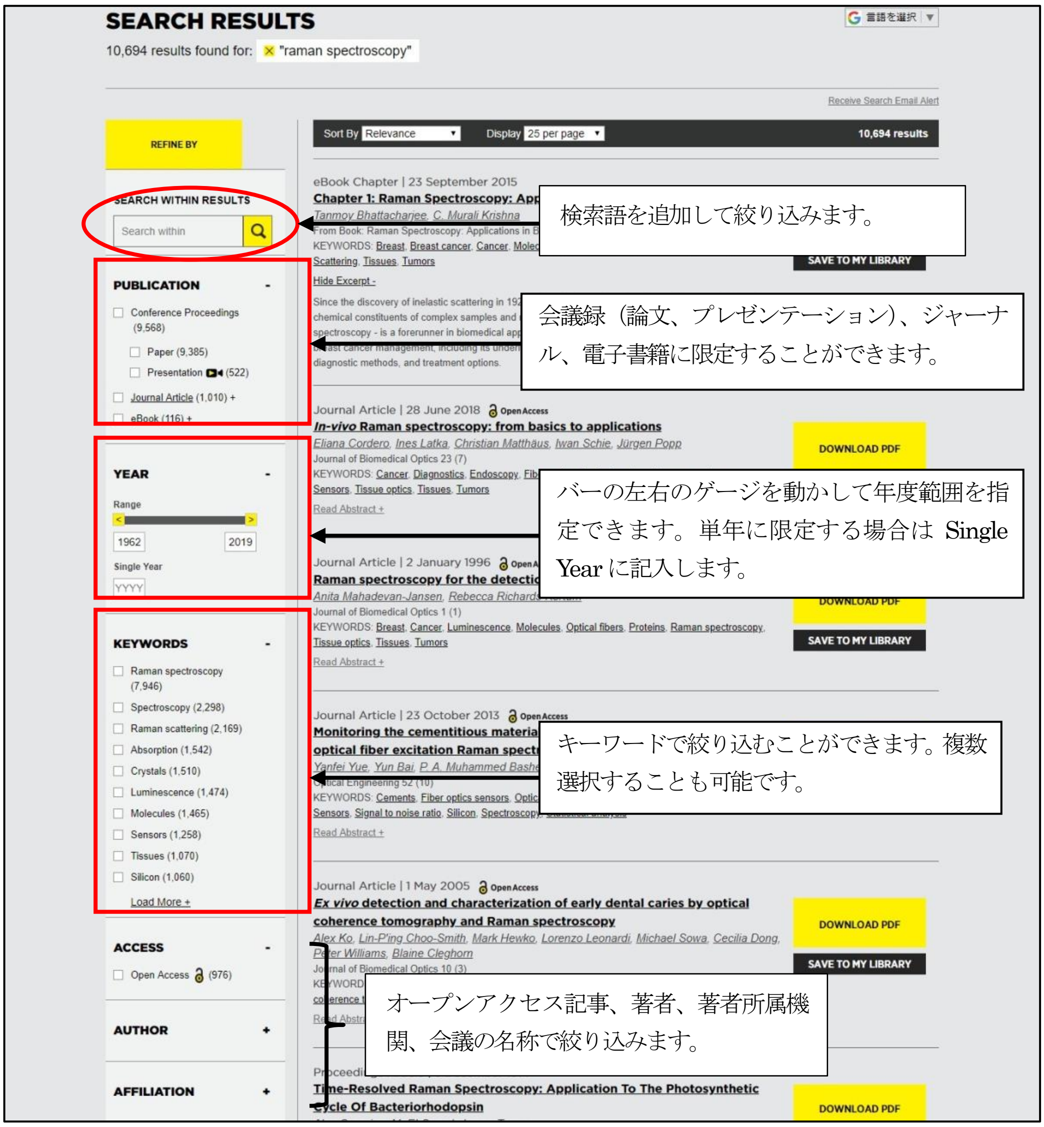

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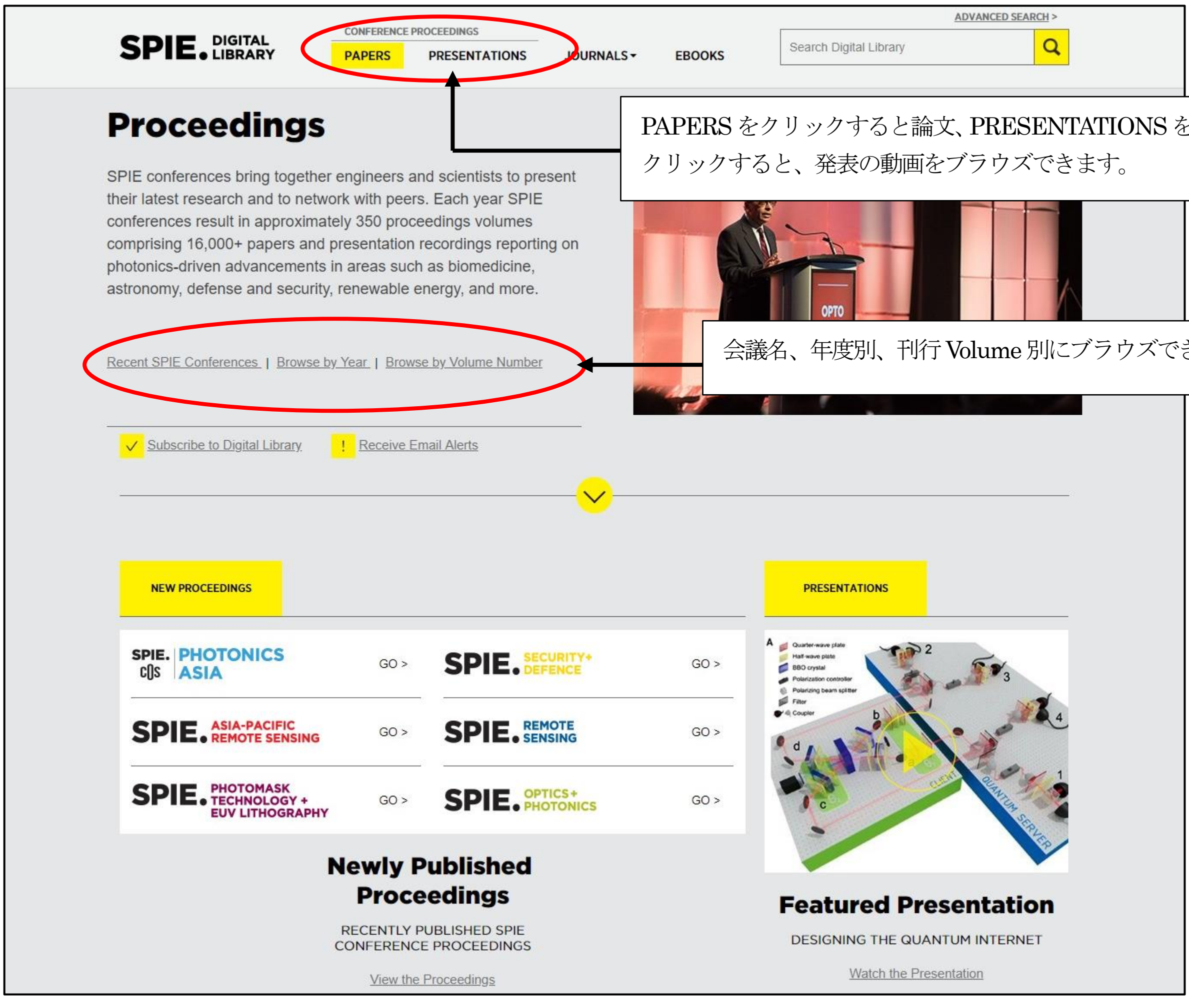

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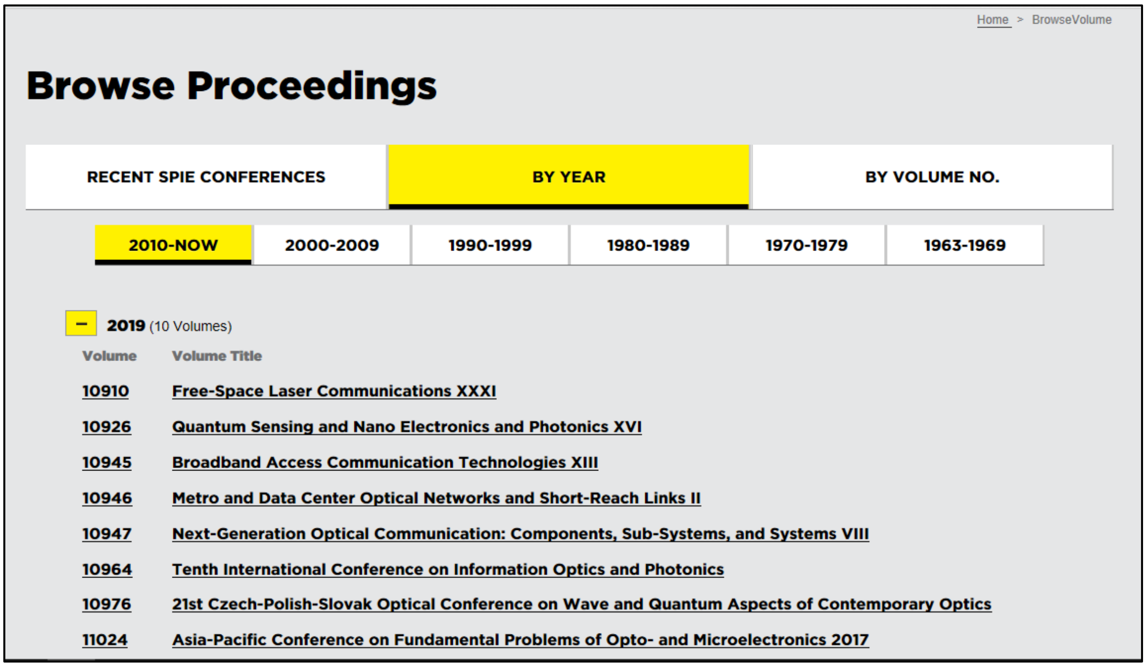

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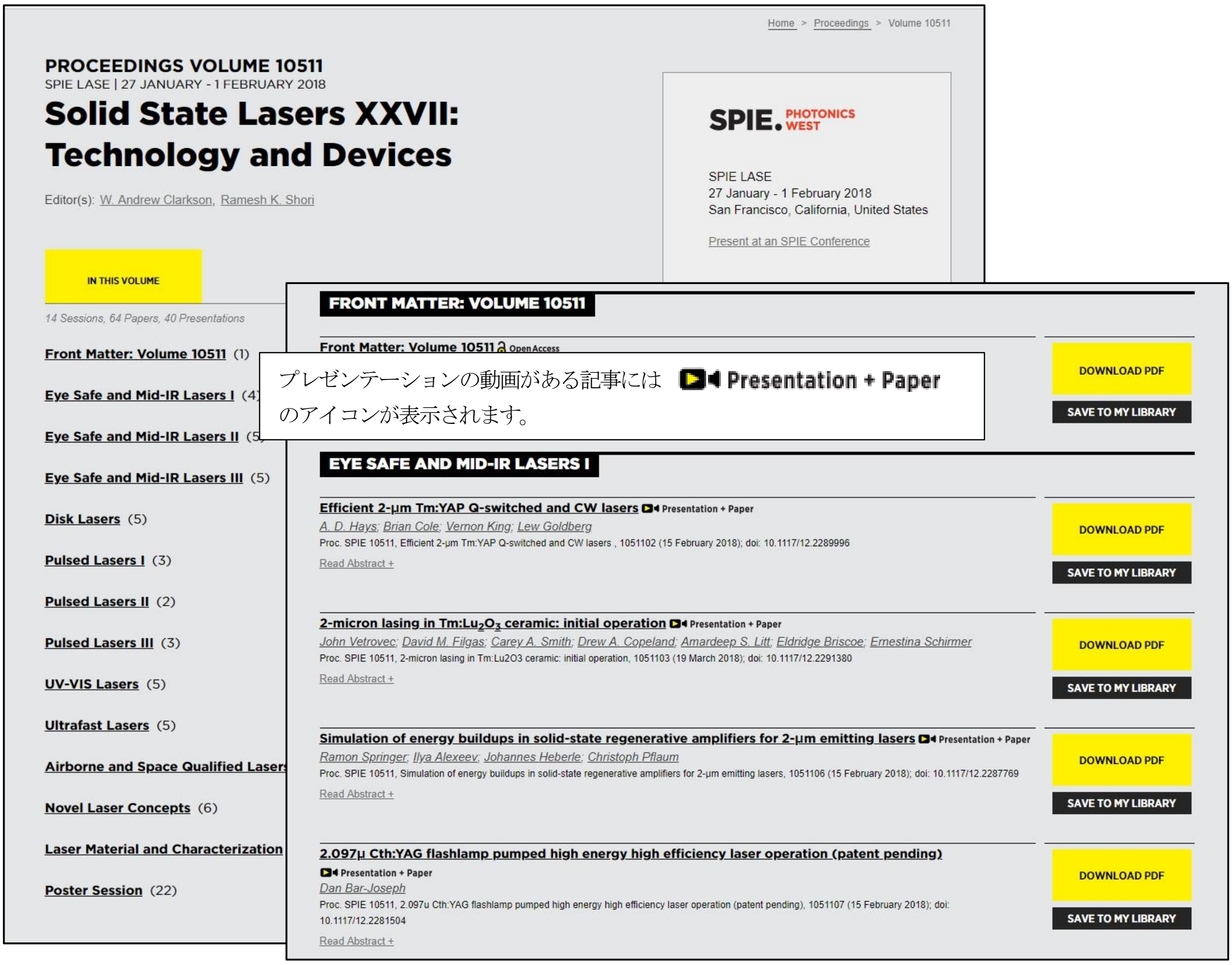

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SPIE LASE | 27 JANUARY - 1 FEBRUARY 2018

Solid State Lasers XXVII: Technology and Devices

Editor(s): W. Andrew Clarkson, Ramesh K. Shori

SPIE LASE
27 January - 1 February 2018
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FRONT MATTER: VOLUME 10511

Front Matter: Volume 10511

EYE SAFE AND MID-IR LASERS I

Efficient 2-μm Tm:YAP Q-switched and CW lasers Presentation + Paper
A. D. Hays; Brian Cole; Vernon King; Lew Goldberg
Proc. SPIE 10511, Efficient 2-μm Tm:YAP Q-switched and CW lasers , 1051102 (15 February 2018); doi: 10.1117/12.2289996
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2-micron lasing in Tm:Lu$_2$O$_3$ ceramic: initial operation Presentation + Paper
John Vetrovec; David M. Filgas; Carey A. Smith; Drew A. Copeland; Amardeep S. Litt; Eldridge Briscoe; Ernestina Schirmer
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Ramon Springer; Ilya Alexeev; Johannes Heberle; Christoph Pflaum
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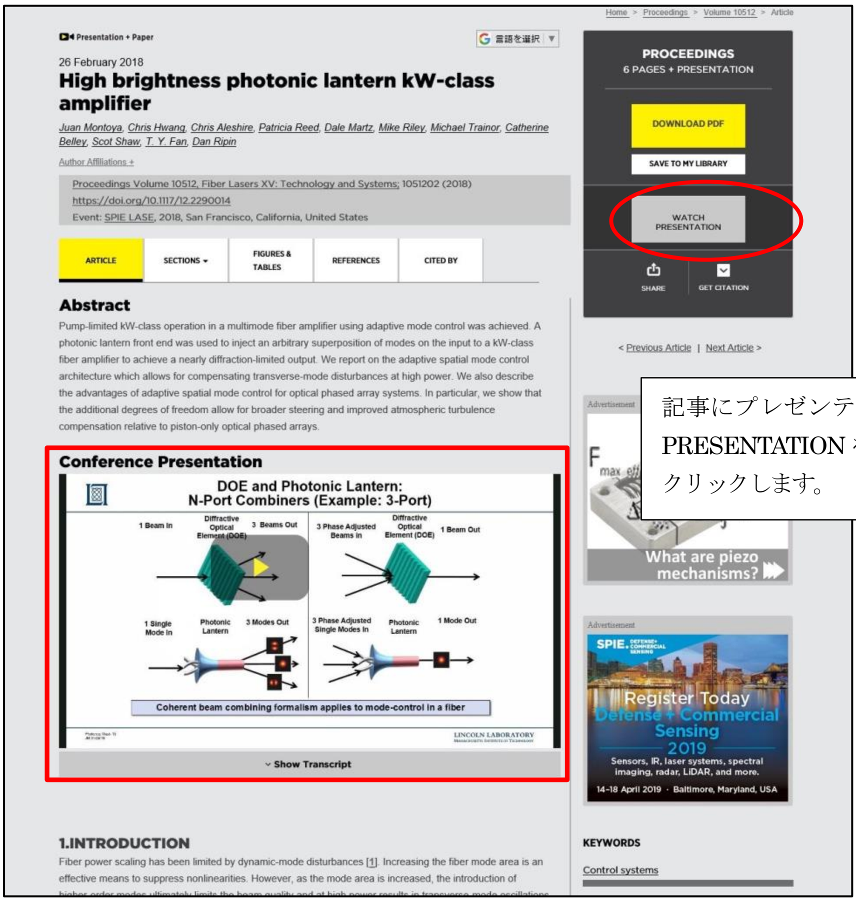

Presentation + Paper

26 February 2018

High brightness photonic lantern kW-class amplifier

Juan Montoya, Chris Hwang, Chris Aleshire, Patricia Reed, Dale Martz, Mike Riley, Michael Trainor, Catherine Belley, Scot Shaw, T. Y. Fan, Dan Ripin

Author Affiliations +

Proceedings Volume 10512, Fiber Lasers XV: Technology and Systems; 1051202 (2018)
https://doi.org/10.1117/12.2290014
Event: SPIE LASE, 2018, San Francisco, California, United States

Abstract

Pump-limited kW-class operation in a multimode fiber amplifier using adaptive mode control was achieved. A photonic lantern front end was used to inject an arbitrary superposition of modes on the input to a kW-class fiber amplifier to achieve a nearly diffraction-limited output. We report on the adaptive spatial mode control architecture which allows for compensating transverse-mode disturbances at high power. We also describe the advantages of adaptive spatial mode control for optical phased array systems. In particular, we show that the additional degrees of freedom allow for broader steering and improved atmospheric turbulence compensation relative to piston-only optical phased arrays.

Conference Presentation

1.INTRODUCTION

Fiber power scaling has been limited by dynamic-mode disturbances [1]. Increasing the fiber mode area is an effective means to suppress nonlinearities. However, as the mode area is increased, the introduction of

KEYWORDS

Control systems

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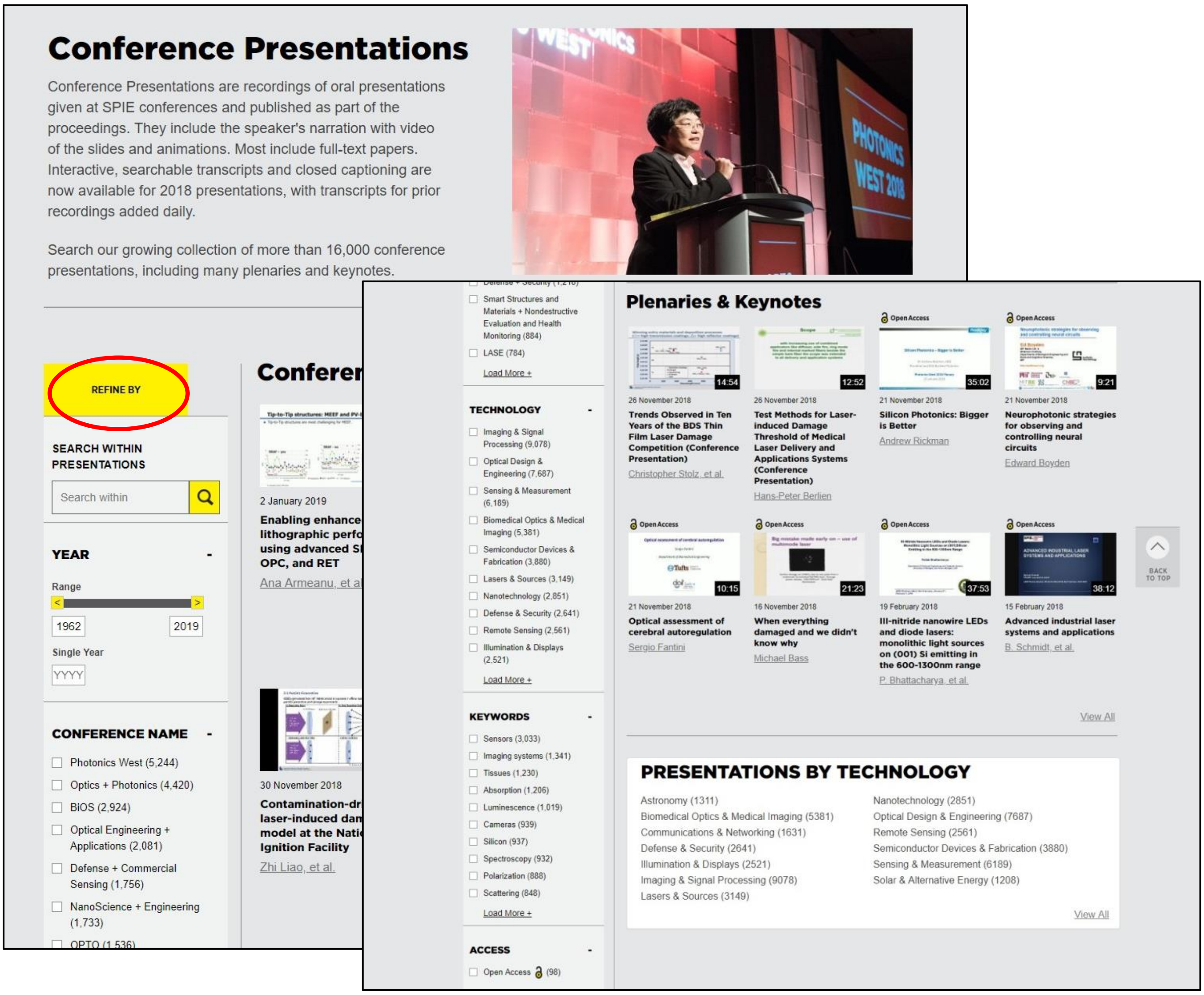

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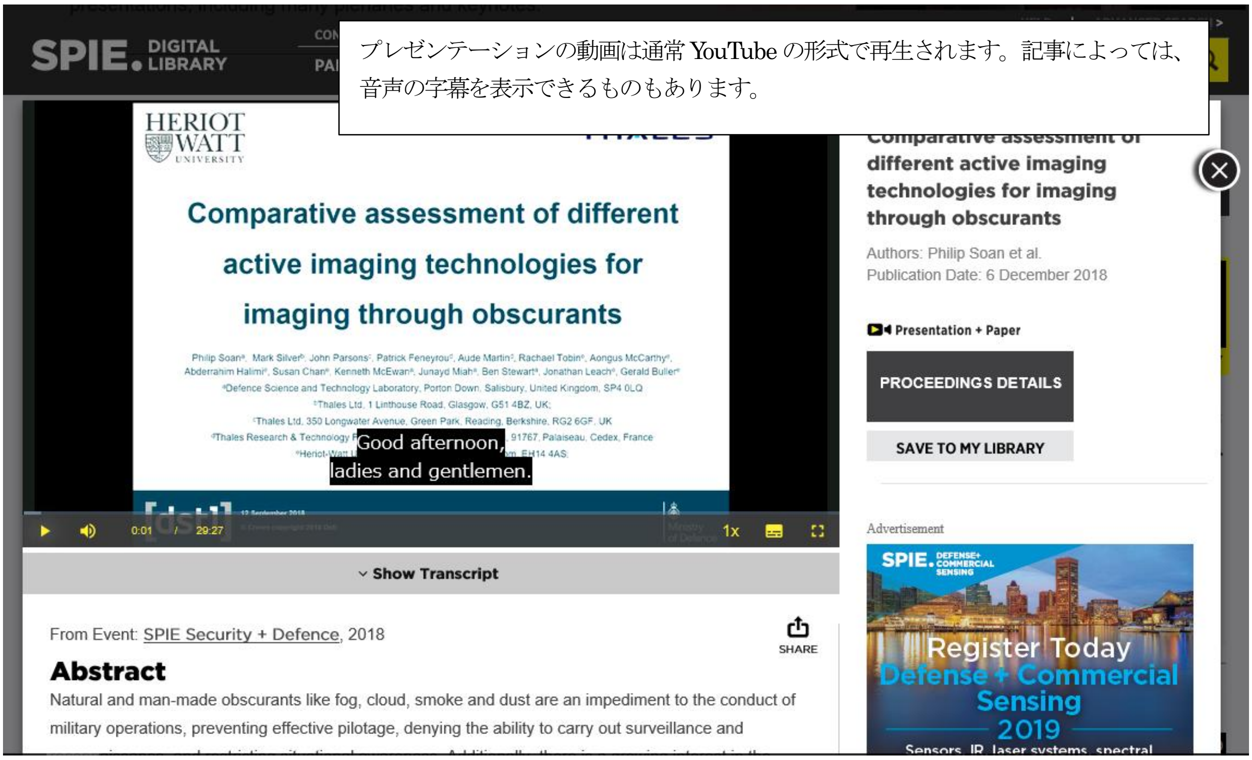

Comparative assessment of different active imaging technologies for imaging through obscurants

Philip Soan[a], Mark Silver[b], John Parsons[c], Patrick Feneyrou[d], Aude Martin[d], Rachael Tobin[e], Aongus McCarthy[e], Abderrahim Halimi[e], Susan Chan[e], Kenneth McEwan[a], Junayd Miah[a], Ben Stewart[a], Jonathan Leach[e], Gerald Buller[e]
[a]Defence Science and Technology Laboratory, Porton Down, Salisbury, United Kingdom, SP4 0LQ
[b]Thales Ltd, 1 Linthouse Road, Glasgow, G51 4BZ, UK;
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Good afternoon,
ladies and gentlemen.

Comparative assessment of different active imaging technologies for imaging through obscurants

Authors: Philip Soan et al.
Publication Date: 6 December 2018

Presentation + Paper

From Event: SPIE Security + Defence, 2018

Abstract

Natural and man-made obscurants like fog, cloud, smoke and dust are an impediment to the conduct of military operations, preventing effective pilotage, denying the ability to carry out surveillance and

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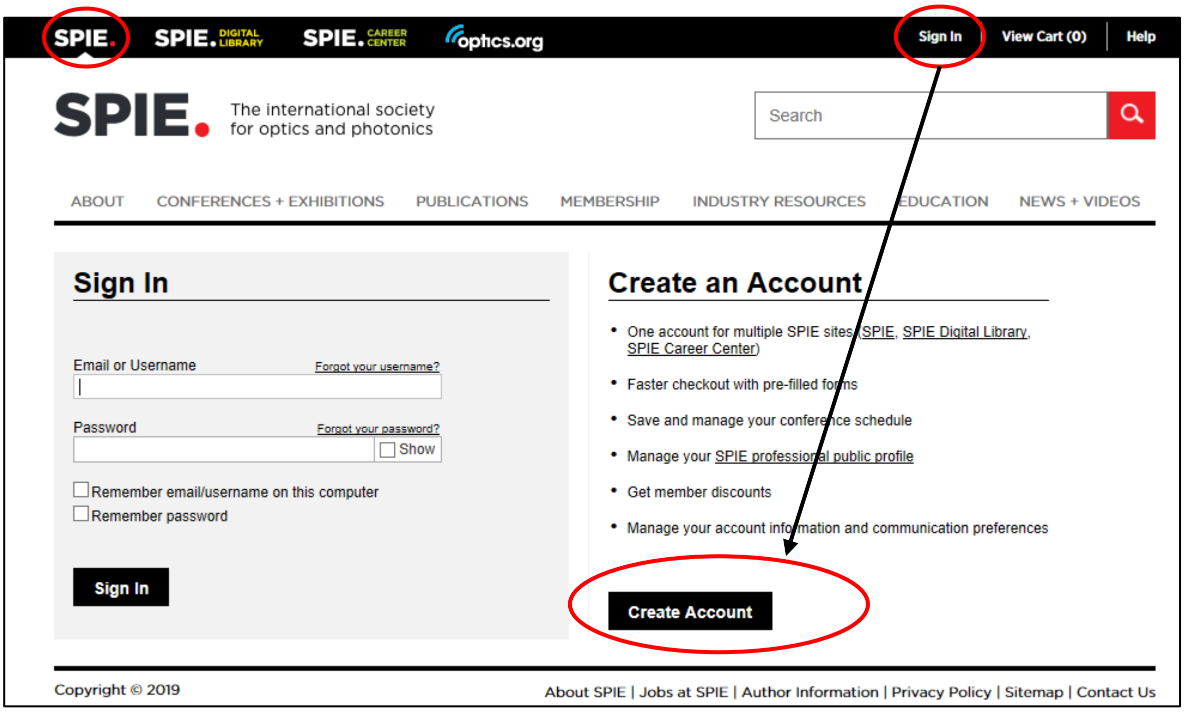

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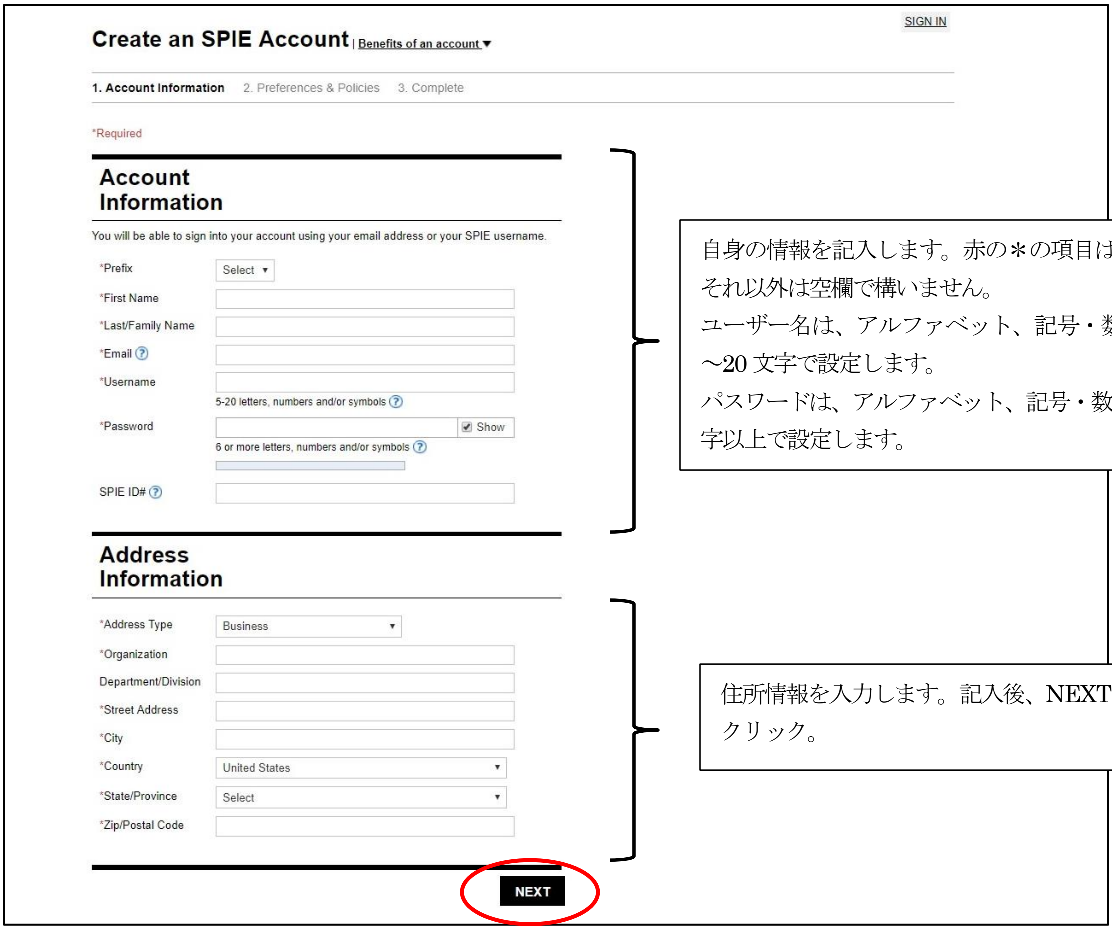

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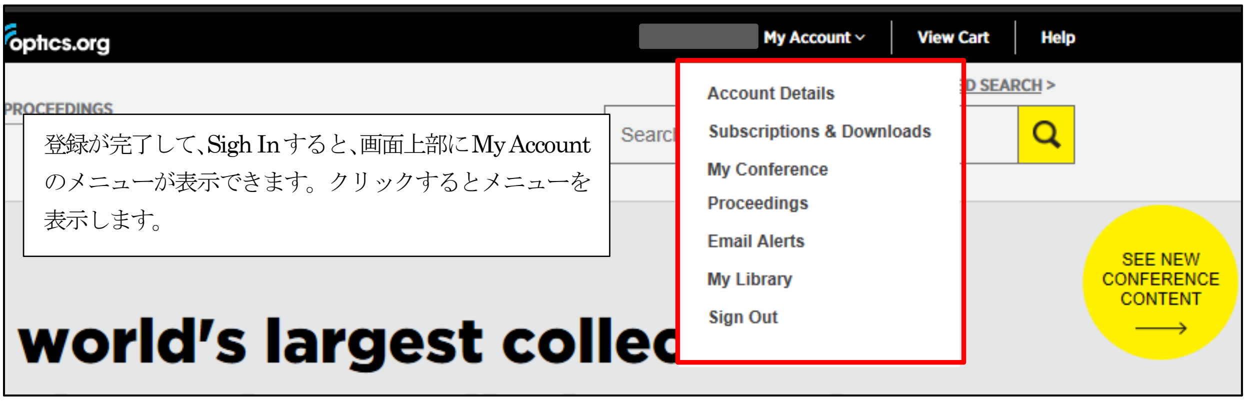

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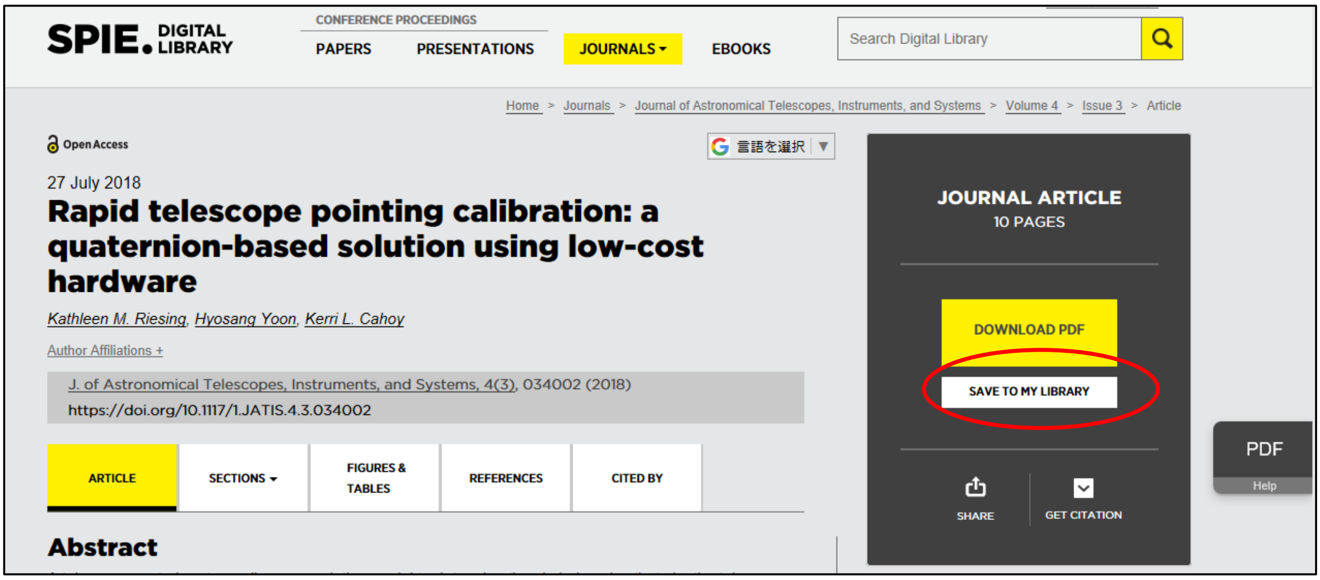

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Rapid telescope pointing calibration: a quaternion-based solution using low-cost hardware

Kathleen M. Riesing, Hyosang Yoon, Kerri L. Cahoy

Author Affiliations +

J. of Astronomical Telescopes, Instruments, and Systems, 4(3), 034002 (2018)
https://doi.org/10.1117/1.JATIS.4.3.034002

Abstract

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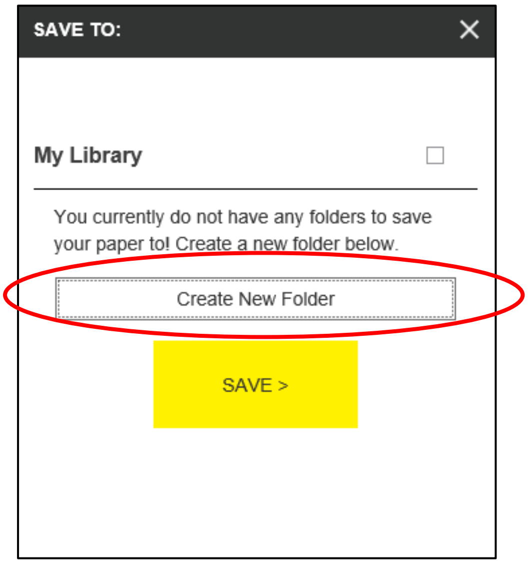

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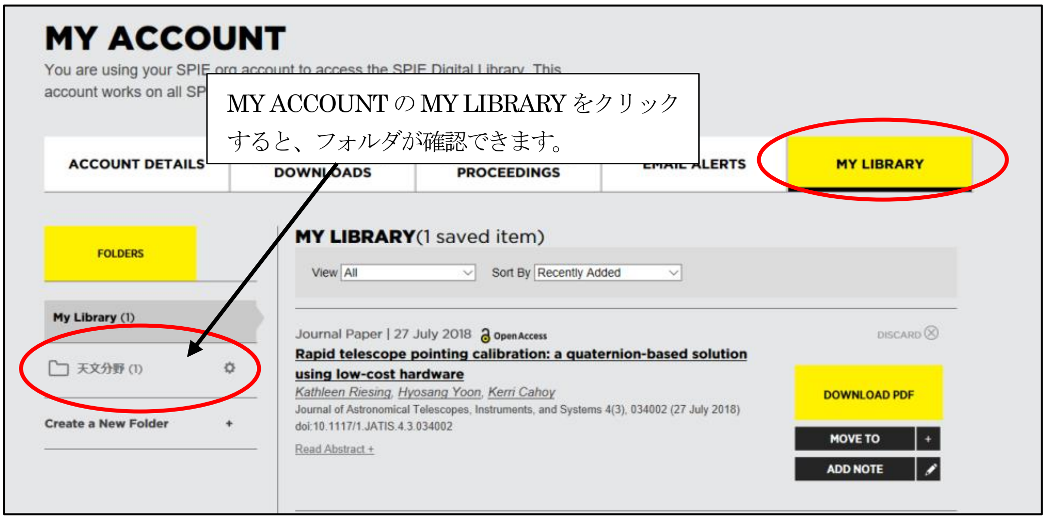

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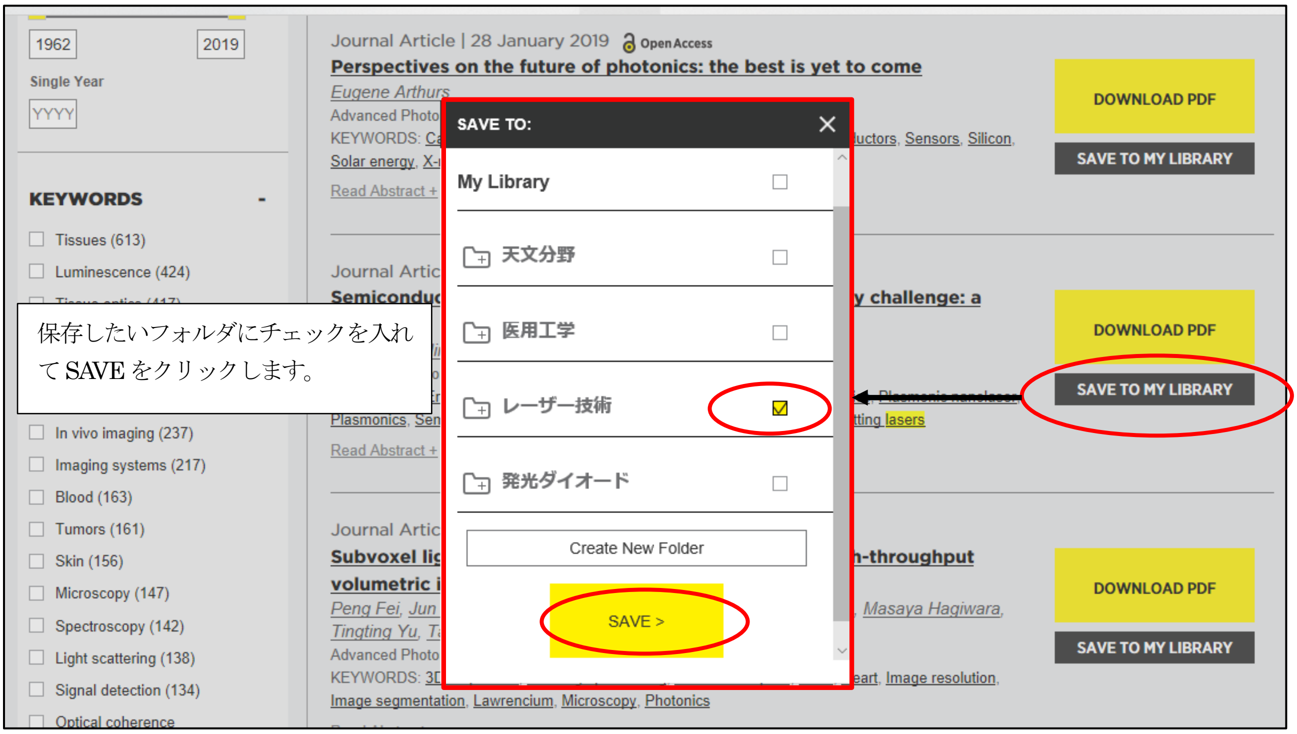

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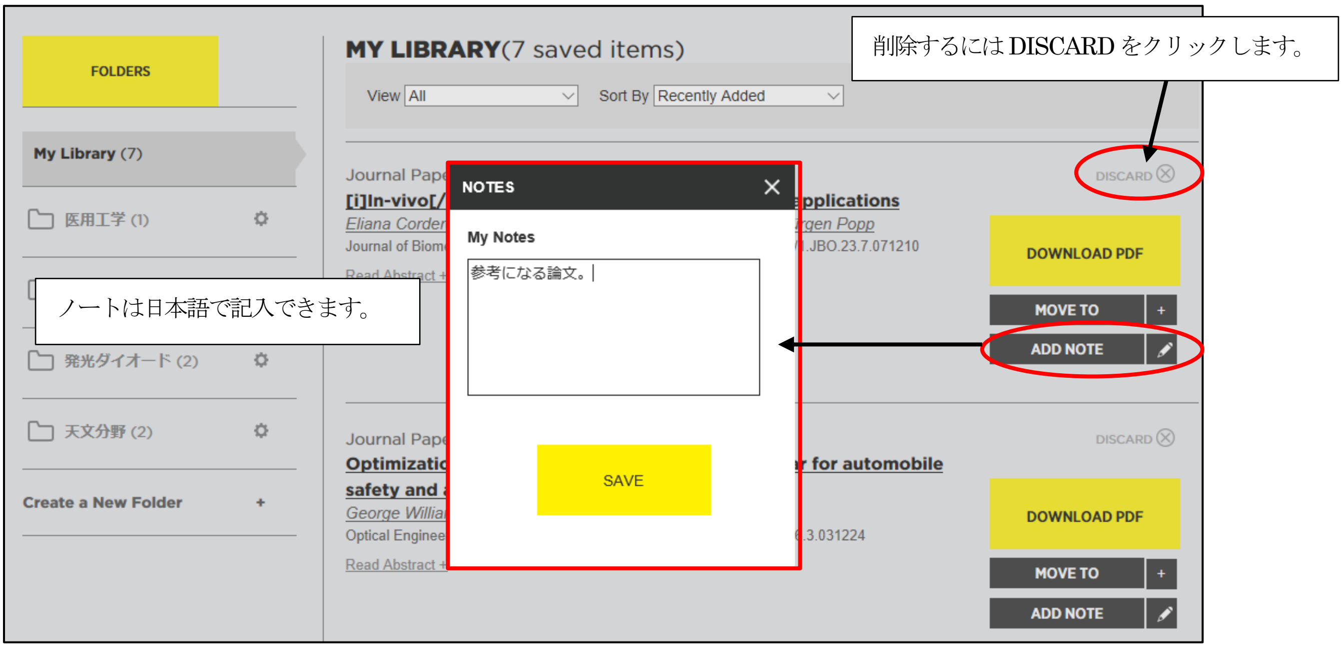

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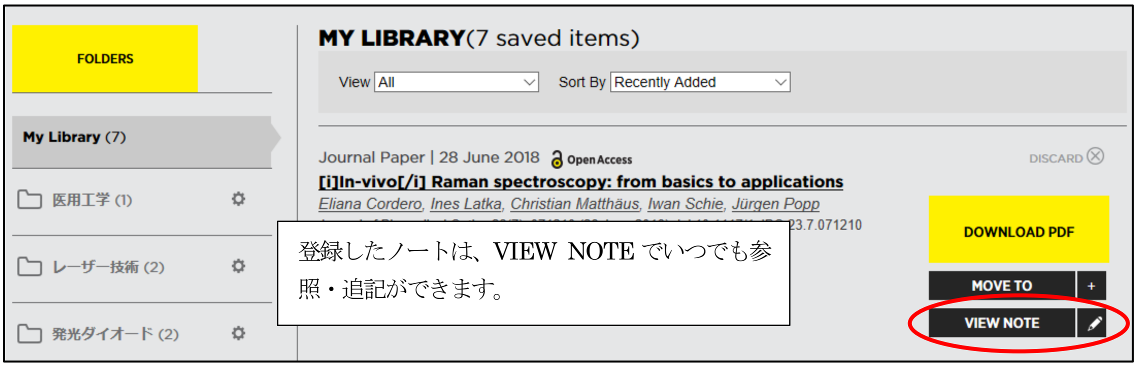

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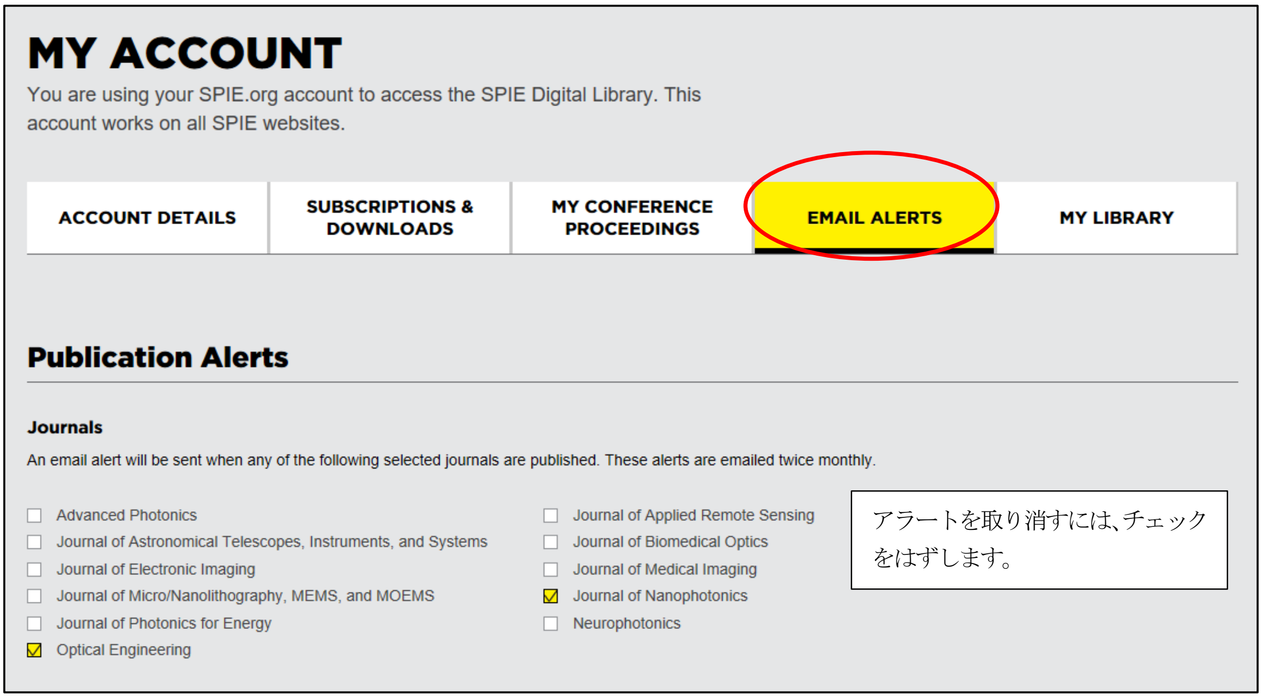

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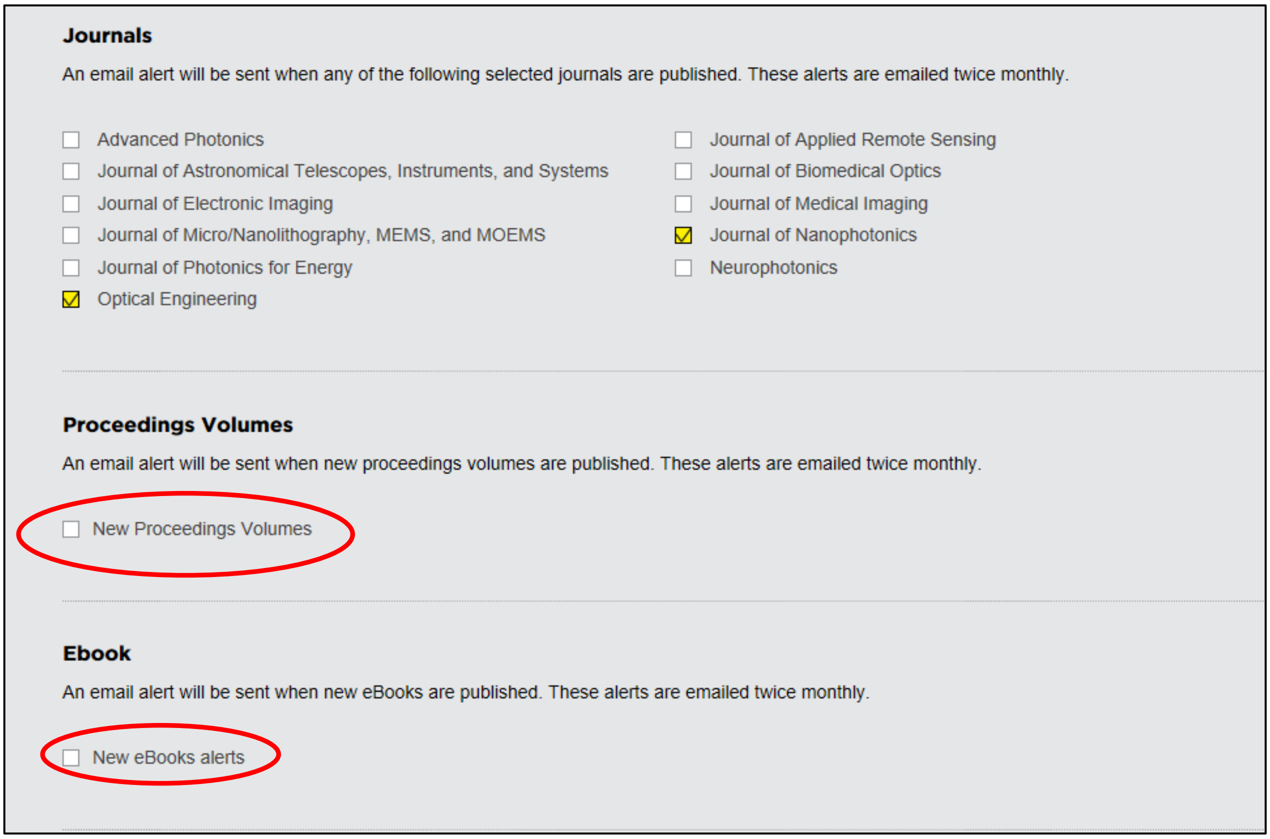

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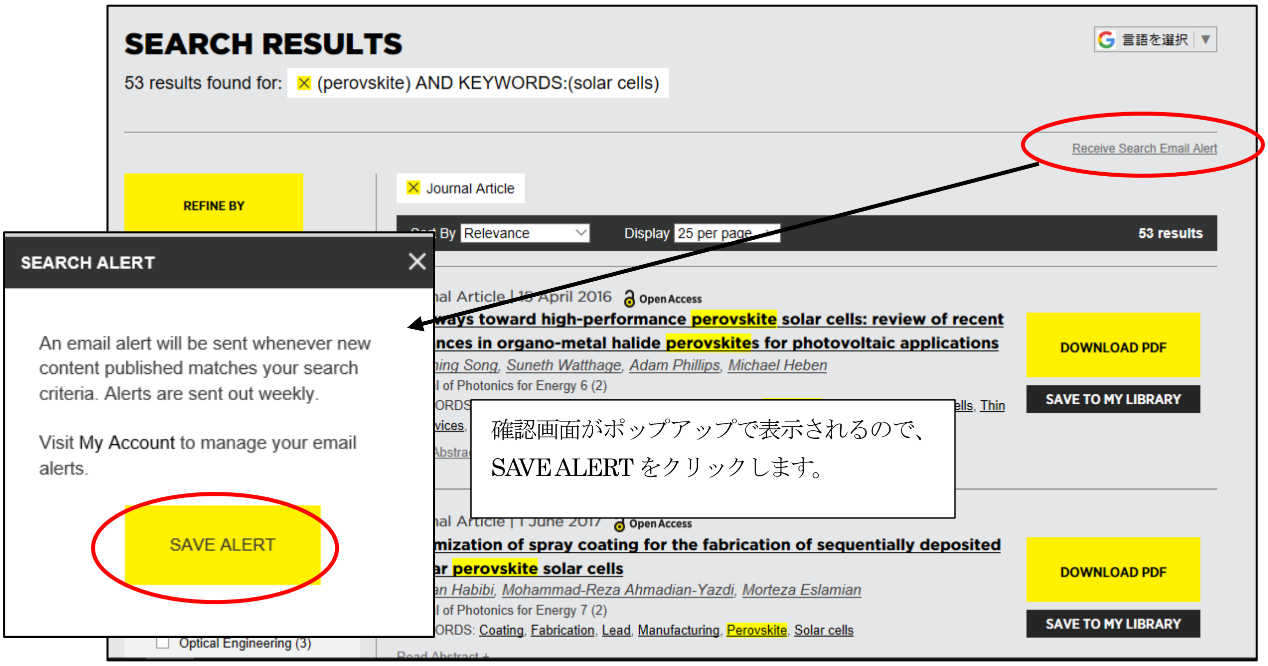

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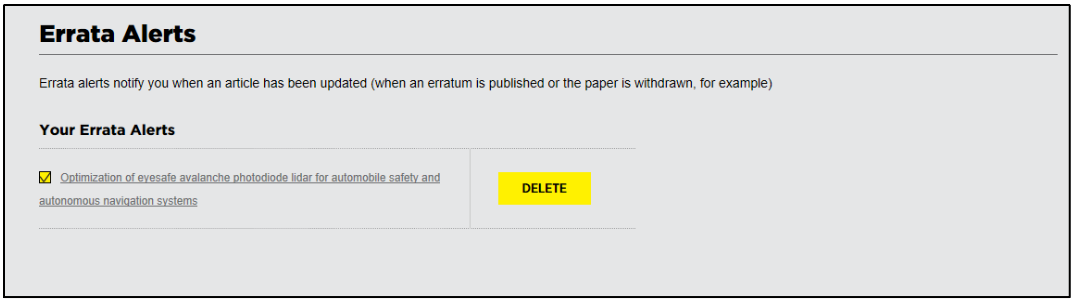

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